



FR

DÉCLARATION DES PERFORMANCES

DoP W0009

pour vis fischer PowerFast II

1. Code d'identification unique du type de produit:	DoP W0009	
2. <u>Usage(s) prévu(s):</u>	Vis autoforeuses pour utilisation dans les annexes 1, 2.	constructions bois, voir annexes, en particulier les
3. <u>Fabricant:</u>	fischerwerke GmbH & Co. KG, Klaus-Fisch	er-Str. 1, 72178 Waldachtal, Allemagne
4. <u>Mandataire:</u>	-	
 Système(s) d'évaluation et de vérification de la constance des performances: 	3	
6. Document d'évaluation européen:	EAD 130118-01-0603	
Evaluation Technique Européenne:	ETA-19/0175; 2021-08-09	
Organisme d'évaluation technique:	ETA-Danmark A/S	
Organisme(s) notifié(s):	2699 Universität Innsbruck	
7. Performance(s) déclarée(s):		
Résistance mécanique et stabilité (BWR 1), Sécurit	té d'utilisation et accessibilité (BWR 4)	
Dimensions:		Annexes 17-24
Moment caractéristique d'écoulement plastique:		Annexe 6
Angle de flexion:		Annexe 3
Paramètre d'arrachement caractéristique:		Annexes 6-8
Paramètre caractéristique de résistance à la travers	sée de la tête de vis:	Annexe 9
Résistance caractéristique en traction:		Annexes 3, 9
Limite d'élasticité caractéristique:		Annexe 6
Résistance caractéristique à la torsion:		Annexe 3
Couple de vissage:		Annexe 3
Entraxes, distances à l'extrémité et au bord des vis	et épaisseur mini du matériau en bois:	Annexes 11-14
Module de glissement pour les vis principalement s	ollicitées axialement:	Annexe 11
Résistance à la corrosion:		Annexe 15
Sécurité en cas d'incendie (BWR 2)		
Réaction au feu:		Classe (A1)
8. Documentation technique appropriée et/ou	-	

8. Documentation technique appropriée et/ou documentation technique spécifique:

Les performances du produit identifié ci-dessus sont conformes aux performances déclarées. Conformément au règlement (UE) no 305/2011, la présente déclaration des performances est établie sous la seule responsabilité du fabricant mentionné ci-dessus.

Signé pour le fabricant et en son nom par:

U.f.

Dr.-Ing. Oliver Geibig, Directeur Général Business Units & Ingénierie Tumlingen, 2021-08-16

Jürgen Grün, Directeur Général Chimie & Qualité

Cette DoP a été préparée en plusieurs langues. En cas de différend relatif à l'interprétation, la version anglaise prévaudra.

L'annexe comprend des informations volontaires et complémentaires en langue anglaise dépassant les exigences légales (spécifiées de manière neutre).

II SPECIFIC PART OF THE EUROPEAN TECHNICAL ASSESSMENT

1 Technical description of product

»fischer PowerFast II« screws are self-tapping screws to be used in timber structures. They shall be threaded over a part of the length or over the whole length. The screws shall be produced from carbon steel wire for nominal diameters between 3,0 mm and 6,0 mm. Where corrosion protection is required, the material or coating shall be declared in accordance with the relevant specification given in Annex A of EN 14592.

The FAFS-Clip are made of zinc die cast for »fischer PowerFast II« screws with countersunk head and a diameter of 5,0 mm.

Geometry and Material

The nominal diameter d (outer thread diameter) of the screws shall not be less than 3,0 mm and not greater than 6,0 mm.

The overall length l_s of the screws, shall not be less than 20 mm and shall not be greater than 300 mm. Dimensions see Annex A.

The ratio of inner thread diameter to outer thread diameter d_1/d ranges from 0,50 to 0,80.

The screws are threaded over a minimum length l_g of 4,0 · d (i.e. $l_g \ge 4,0$ · d).

The thread pitch p (distance between two adjacent thread flanks) ranges from $0,50 \cdot d \text{ to } 0,85 \cdot d$.

No breaking shall be observed at a bending angle of $\alpha \le (45/d^{0.7} + 20)^\circ$.

2 Specification of the intended use in accordance with the applicable EAD

The screws are used for connections in load bearing timber structures between members, softwood and hardwood of: Solid Timber (C), Glued-Laminated Timber (GL), Cross-Laminated Timber (CLT) and Laminated Veneer Lumber (LVL), similar glued members, Wood-Based Panels or steel. »fischer PowerFast II« screws with a thread over the full length can also be used as tensile or compressive reinforcement perpendicular to the grain or as shear reinforcement. Furthermore »fischer PowerFast II«

screws with diameter of 6 mm may also be used for fixing of thermal insulation on rafters and on vertical

facades and 5 mm screws can be combined with the FAFS-Clip.

Steel plates, wood-based panels and plasterboards shall only be fixed on the side of the screw head. The minimum thickness of wood-based panels should be $1,2 \cdot d$.

The following wood-based panels can be used:

- Plywood according to EN 636 or European Technical Assessment or national provisions that apply at the installation site
- Particleboard according to EN 312 or European Technical Assessment or national provisions that apply at the installation site
- Oriented Strand Board (OSB) according to EN 300 or European Technical Assessment or national provisions that apply at the installation site
- Fibreboard according to EN 622-2, EN 622-3 and EN 622-5 or European Technical Assessment (minimum density 650 kg/m³) or national provisions that apply at the installation site
- Cement-bonded particleboard according to EN 634, European Technical Assessment or national provisions at the installation site
- Solid wood panels according to EN 13353 or European Technical Assessment or national provisions that apply at the installation site
- Wood-based panels for use in constructions according to EN 13986
- Cross-Laminated Timber (CLT) according to European Technical Assessment
- Laminated Veneer Lumber (LVL) according to EN 14374 or European Technical Assessment
- Engineered wood products according to European Technical Assessments, provided that the ETA for the product provides provisions for the use of selftapping screws and these provisions are applied

The screws shall be driven into softwood and hardwood with a maximum characteristic density of 730 kg/m³ without pre-drilling or after pre-drilling (see Table 1 and Table 2) with a diameter not larger than the inner thread diameter for the length of the threaded part and with a maximum of the smooth shank diameter for the length of the smooth shank.

Table 1: Recommended pre-drilling diameters			
Nominal diameter	Bore-hole diameter [mm]		
<i>d</i> [mm]	Softwood	Hardwood	
3,0	2,0	2,5	
3,5	2,0	2,5	
4,0	2,5	3,0	
4,5	2,5	3,0	
5,0	3,0	3,0	
6,0	4,0	4,0	

Recommended values without pre-drilling for the maximum penetration length of the threaded part of »fischer PowerFast II« made of carbon steel in wood-based members like ash, beech and oak or LVL according to ETA-14/0354 (e.g. Baubuche) are shown in Table 2. The FAFS-Clip can be installed with or without pre-drilling (see chapter 3.7.11), recommended borehole diameter 5 mm.

without pre-drilling in hardwood		
Nominal diameter Maximum penetration		
<i>d</i> [mm]	length [mm]	
3,0	40	
3,5	45	
4,0	50	
4,5	60	

5.0

6,0

Table 2: Recommended penetration length

To fix steel parts with the head side of the screw, the boreholes must be pre-drilled with a suitable diameter.

70

70

When using screws with a countersunk, step countersunk and raised countersunk head, the upper surface of the screw head must be flush with the surface of the timber part. Countersinking deeper is not permitted and should be avoided, because of damaging the surface and reduce the durability of the construction. Countersunk head screws made of carbon steel according to Annex A1 and A2 can be used together with washers according to Annex A8. Washers according to EN ISO 7094 can be used together with washers according to Annex A8.

For the use of screws in the edge side of wood-based panels one have to pre-drill with a diameter not larger than the inner thread diameter for the length of the threaded part and with a maximum of the smooth shank diameter for the length of the smooth shank.

Pan head, step countersunk and washer head screws according to Annex A3, A4 and A5, may be used together with washers according to EN ISO 7094.

»fischer PowerFast II« screws can be driven in with standard screw drillers and with torque impact screw drivers too (e.g. fischer FSS 18V 400 BL or fischer FSS 18V 600). In combination with steel plates, torque controlled tools e.g. torque wrenches have to be used. For the use of screws in wood-based panels, like particle- and fibreboards, the screws have to be tightened carefully to ensure the characteristic load bearing capacity.

The design of the connections shall be based on the characteristic load-carrying capacities of the screws. The design capacities shall be derived from the characteristic capacities in accordance with Eurocode 5 or an appropriate national code. The screws are intended for the use of connections subjected to static or quasi-static loadings.

The zinc-coated screws are for the use in timber structures subjected to the moisture defined by the service classes 1 and 2 according to EN 1995-1-1.

The intended use of the screws is in timber connections for which all requirements of mechanical resistance, stability and safety in use in the sense of the Basic Works Requirements 1 and 4 of Regulation 305/2011 (EU) shall be fulfilled.

The provisions made in this European Technical Assessment are based on an assumed intended working life of the screws of 50 years.

The indications given on the working life cannot be interpreted as a guarantee given by the producer or Assessment Body, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the products.

3 Performance of the product and references to the methods used for its assessment

Characteristic	Assessment of characteristic	
3.1 Mechanical resistance and stability (BWR1)		
Characteristic yield moment Characteristic withdrawal parameter Characteristic head pull-trough parameter of screws Characteristic yield strength Insertion moment Spacing, end and edge distances Slip modulus	See section 3.7 to 3.9	
Bending angle	No breaking has been observed at a bending angle of $\alpha \le 45^{\circ}/d^{0,7}+20^{\circ}$	
Tensile strength PowerFast II	Characteristic value $f_{tens,k}$: d= 3,0 mm 3,2 kN d= 3,5 mm 4,1 kN d= 4,0 mm 5,2 kN d= 4,5 mm 6,3 kN d= 5,0 mm 8,9 kN d= 6,0 mm 13,1 kN	
Torsional strength PowerFast II	Characteristic value $f_{tor,k}$: d= 3,0 mm 1,5 Nm d= 3,5 mm 2,0 Nm d= 4,0 mm 3,0 Nm d= 4,5 mm 4,2 Nm d= 5,0 mm 6,0 Nm d= 6,0 mm 10,0 Nm Note: Ratio of the characteristic torsional strength to the mean insertion moment: $f_{tor,k} / R_{tor,mean} \ge 1,5$	
3.2 Safety in case of fire (BWR2)		
Reaction to fire	The screws are made from steel classified as Performance Class A1 of the characteristic reaction to fire, in accordance with the provisions of Commission Delegated Regulation 2016/364 and EC decision 96/603/EC, amended by EC Decision 2000/605/EC.	
3.3 Safety in use (BWR4)	See aspects covered by BWR1	
3.4 Durability against corrosion	The screws have been assessed as having satisfactory durability and serviceability when used in timber structures using the timber species described in EN 1995-1-1 and subjected to the conditions defined by service classes 1 and 2	
3.5 Identification	See Annex A	
3.6 Typical and special application area	See Annex B	

3.7 Mechanical Resistance and Stability

The load-carrying capacities for the »fischer PowerFast II« screws are applicable to the woodbased materials mentioned in paragraph 1 even though the term "timber" has been used in the following. European Technical Assessments for structural members or wood-based panels must be considered if applicable.

The characteristic lateral load-carrying capacities and the characteristic axial withdrawal capacities of »fischer PowerFast II« screws should be used for designs in accordance with Eurocode 5 (EN 1995-1-1) or an appropriate valid national code.

Reductions in the cross-sectional area caused by »fischer PowerFast II« screws shall be taken into account in accordance to the Eurocode 5.

3.7.1 Lateral load-carrying capacity $f_{h,k}$

The characteristic lateral load-carrying capacity of »fischer PowerFast II« screws shall be calculated according to EN 1995-1-1. The contribution of the rope effect may be considered. For the calculation of the load-carrying capacity, the following parameters should be taken into account.

3.7.1.1 Embedment strength $f_{h,a,k}$ for use in Solid Timber (EN 338, EN 15497) and Glued-Laminated Timber (EN 14080)

The embedment strength for »fischer PowerFast II« screws in non-pre-drilled holes arranged at an angle between load and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$ can be calculated with the help of equation (1).

$$f_{h,k} = 0,082 \cdot \rho_k \cdot d^{-0,3} \tag{1}$$

The embedment strength for »fischer PowerFast II« screws in pre-drilled holes arranged at an angle between load and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$ can be calculated with the help of equation (2).

$$f_{h,\alpha,k} = 0,082 \cdot \rho_k \cdot (1 - 0,01 \cdot d)$$
 (2)

Note: For the calculation according to the EN 1995-1-1 for the calculation of the effective diameter the nominal diameter d should be used.

Screws parallel to the end-grain direction are only allowed for short-time loads and can be calculated with the help of equation (3).

$$f_{h,k} = 0,0076 \cdot \rho_k^{1,24} \cdot d^{-0,3}$$
(3)

Where

- α Angle between load and the grain direction [°]
- $f_{h,k}$ Characteristic embedment strength [N/mm²]
- ρ_k Characteristic timber gross density [kg/m³]
- *d* Nominal diameter of the screw [mm]

3.7.1.2 Embedment strength $f_{h,\alpha,k}$ for use in Cross-Laminated Timber

If there are no other technical specification (ETA or hEN) for Cross-Laminated Timber (CLT), the embedment strength for screws can be calculated as following. The following specifications are only for screws with a diameter of at least 5 mm, otherwise possible influences of gaps between the single lamellas have to be considered.



Figure 1: Notations CLT-elements

- (1) Element plane
- (2) Plane surface
- (3) Edge surface (Narrow side)
- (4) Inner layer (Inner lamellas)
- (5) Outer layer (Outer lamellas)
- (6) Middle layer (Middle lamella)

Screws in the plane surface

The embedment strength for screws in the plane surface of CLT-elements should be assumed as for solid timber according to equation (1) or (2), based on the characteristic density of the outer layer. If relevant, the angle between force and grain direction of the outer layer should be considered.

Screws in the narrow (edge) side

The embedment strength for screws in the narrow side of CLT-elements should be assumed according to equation (4).

$$f_{h,k} = 20 \cdot d^{-0.5} \tag{4}$$

3.7.1.3 Embedment strength $f_{h,\alpha,k}$ for use in Laminated Veneer Lumber according to (ETA-14/0354)

The embedment strength for »fischer PowerFast II« screws with $d \ge 5$ mm arranged at an angle between load and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$ can be calculated with the help of equation (5) in direction 90|90 (see figure 2).

$$f_{h,\alpha,k} = \frac{f_{h,0,k}}{(0,9+0,037\cdot d)\cdot \sin^2 \alpha + \cos^2 \alpha}$$
(5)

With

 $d = 5,0 \text{ mm:} \qquad f_{h,0,k} = 50,0 \text{ N/mm}^2 \\ d = 6,0 \text{ mm:} \qquad f_{h,0,k} = 46,0 \text{ N/mm}^2$

3.7.1.4 Embedment strength $f_{h,\alpha,k}$ for the use in Wood-Based Panels and Plasterboards

The embedment strength for »fischer PowerFast II« screws in non-pre-drilled holes, if no other descriptions are given in Table 3, arranged at an angle α =90° to the plane surface can be calculated with equation (6).

$$f_{h,k} = f_{h,90|90,k} \tag{6}$$

Where

d	Nominal diameter of the screw [mm]
t	Minimum value of the thickness of the
	wood-based panels/plasterboards or
	effective penetration depth of the screw
	[mm]
With	

 $f_{h,90|90,k}$ Characteristic value of the embedment strength according to Table 3 and Figure 3; the influence of load-grain direction is negligible N/mm²]

Table 3: Characteristic values of the embedment strength	
of »fischer PowerFast II« screws in the plane surface	

of »fischer PowerFast II« se	crews in the pl	ane surface
Material		$[N/mm^2]$
OSB		
t > 5 mm	$f_{h,90/90,k} =$	$48 \cdot d^{-0,7} \cdot t^{-0,1}$
(EN 300)	5, 5	
EGGER OSB 4 TOP,		
pre-drilled		
t > 10 mm	$f_{h,90/90,k} =$	$50 \cdot d^{-0,6} \cdot t^{0,2}$
(EN 13986)		
EGGER OSB 4 TOP,		
without pre-drilling		
t > 10 mm	$f_{h, 90/90, k} =$	$65 \cdot d^{-0,7} \cdot t^{0,1}$
(EN 13986)		
Plywood		
t > 4 mm	f	$65 \cdot d^{-0,7} \cdot t^{0,1}$
(EN 314-2)	$f_{h, 90/90, k} =$	05
Fibreboards,		
hardboards (HDF) $t > 2$ must	$f_{h,90/90,k} =$	$30 \cdot d^{-0,3} \cdot t^{0,6}$
t > 3 mm	5	
(EN 622-2)		
Fibreboards		
medium boards	$f_{h, 90/90, k} =$	$28 \cdot d^{-0,6} \cdot t^{0,6}$
(MDF)		
t > 3 mm		
(EN 622-3)		
Particleboards		
t > 5 mm	$f_{h, 90/90, k} =$	$50 \cdot d^{-0.6} \cdot t^{0.2}$
(EN 312)		
Gypsum		
plasterboards	ſ	$3,9 \cdot d^{-0,6} \cdot t^{0,7}$
$t \ge 9 \text{ mm}$	$f_{h, 90/90, k} =$	$3,9.d^{\circ,\circ}.t^{\circ,\circ}$
(EN 520)		
Gypsum boards with		
fibrous reinforcement	$f_{h, 90/90, k} =$	$7, 8 \cdot d^{-0,2} \cdot t^{0,7}$
$t \ge 9 \text{ mm}$		
(EN 15283-2)		
(L1(15205-2)		

The embedment strength for »fischer PowerFast II« screws in pre-drilled holes, if no other descriptions are given in Table 4, arranged at an angle $\alpha = 90^{\circ}$ to the edge surface (see Figure 4) in EGGER OSB 4 TOP can be calculated with equation (7).

$$f_{h,k} = f_{h,90|00,k} \tag{7}$$

Where

d t

Nominal diameter of the screw [mm]	
Penetration depth of the screws parallel	Į
to the plane surface in EGGER OSB)
TOP 4 panels [mm]	

With

 $f_{h,90|00,k}$ Characteristic value of the embedment strength; the influence of load-grain direction is negligible see table 4 and figure [N/mm²]

Table 4: Characteristic values of the embedment strength

of »fischer PowerFast II« s	crews in the edg	ge surface
Material		[N/mm ²]
EGGER OSB 4 TOP, pre-drilled t >10 mm Load parallel to plane	$f_{h,90/00,k} =$	$12 \cdot d^{-0,6} \cdot t^{0,2}$
(EN 13986)		
EGGER OSB 4 TOP, without pre-drilling t >10 mm Load parallel to plane (EN 13986)	$f_{h,90/00,k} =$	$16 \cdot d^{-0,7} \cdot t^{0,1}$
EGGER OSB 4 TOP, pre-drilled t >10 mm Load normal to plane (EN 13986)	fh,90/00,k =	$40 \cdot d^{-0,6} \cdot t^{0,2}$
EGGER OSB 4 TOP, without pre-drilling t >10 mm Load normal to plane (EN 13986)	f _{h,90/00,k} =	$52 \cdot d^{-0,7} \cdot t^{0,1}$

3.7.1.5 Effective number of screws per row *n*_{ef}

For laterally loaded screws, the rules for multiple fastener connections in EN 1995-1-1 should be applied.

3.7.2 Yield strength $f_{y,k}$

The characteristic yield strength of the different screw types of »fischer PowerFast II« can be taken into account as shown below.

$$f_{v,k} = 1050 \text{ N/mm}^2$$
 (8)

3.7.3 Yield moment M_{v,Rk}

The characteristic yield moment shall be calculated with the help of equation (9)

$$M_{y,Rk} = 0.15 \cdot 600 \cdot d^{2.65} \tag{9}$$

Where

Characteristic yield moment [Nmm] $M_{v,Rk}$ Nominal diameter of the threaded part [mm] d

3.7.4 Axial withdrawal capacity $f_{ax,k}$

The axial withdrawal capacity is limited by the head pull-through capacity, the withdrawal capacity and the tensile or compressive capacity of the screw.

For »fischer PowerFast II« fully threaded screws, the withdrawal capacity of the thread in the member with the head may be considered instead of the head pull-through capacity.

3.7.4.1 Withdrawal capacity $F_{ax,a,Rk}$ for use in Solid Timber (EN 338, EN 15497), Glued-Laminated Timber (EN 14080) and Laminated Veneer Lumber according to (ETA-14/0354)

In solid timber and glued-laminated timber of softwood, the characteristic withdrawal capacity of »fischer PowerFast II« screws, with an angle of $0^{\circ} \le \alpha \le 90^{\circ}$; shall be calculated according to equation (10).

$$F_{ax,\alpha,Rk} = n_{ef} \cdot k_{ax} \cdot f_{ax,90,k} \cdot d \cdot l_{ef} \cdot \left(\frac{\rho_k}{350}\right)^{0,8}$$
(10)

With

$$k_{ax} = \min \begin{cases} 0, 3 + (0, 7 \cdot \alpha) / 45^{\circ} \\ 1,00 \end{cases}$$
(11)

According to equation (12) the point side penetration length has to be considered between the following ranges.

$$l_{ef} = \min \begin{cases} \frac{4 \cdot d}{\sin \alpha} \\ 20 \cdot d \end{cases}$$
(12)

Where

d Outer thread diameter [mm]

Penetration length of the threaded part l_{ef} according to EN 1995-1-1; For fully threaded screws the thread length including the head length in [mm]

Angle between grain and screw axis [°] α

$$\rho_k$$
 Characteristic timber gross density [kg/m³]

Characteristic withdrawal capacity of the $F_{ax,\alpha,Rk}$ screw with an angle α to the grain [N] Effective number of screws according to nef EN 1995-1-1

With

Characteristic withdrawal parameter, shown fax,90,k in Table 5

Table 5: Characteri	stic withdrawal p	arameters		
PowerFast II	Solid Timber or			
	Glued-Lamin	Glued-Laminated Timber		
d= 3,0 mm	$f_{ax,90,k} =$	15,5 N/mm ²		
d= 3,5 mm	$f_{ax,90,k} =$	14,9 N/mm ²		
d= 4,0 mm	$f_{ax,90,k} =$	14,5 N/mm ²		
d= 4,5 mm	$f_{ax,90,k} =$	14,1 N/mm ²		
d= 5,0 mm	$f_{ax,90,k} =$	13,8 N/mm ²		
d= 6,0 mm	$f_{ax,90,k} =$	12,9 N/mm ²		
PowerFast II	LVL accordi	ng to		
	ETA-14/035	4		
d= 5,0 mm	$f_{ax,90 90,k} =$	40,0 N/mm ²		
	$f_{ax,90 00,k} =$	32,0 N/mm ²		
	$f_{ax,00 00,k} =$	32,0 N/mm ²		
d= 6,0 mm	$f_{ax,90 90,k} =$	32,0 N/mm ²		
	$f_{ax,90 00,k} =$	24,0 N/mm ²		
	$f_{ax,00 00,k} =$	24,0 N/mm ²		
$\alpha = 90 00$		00		
		$\alpha = 90 90$		

Figure 2: PowerFast II in hardwood LVL

The characteristic withdrawal capacity in hardwood LVL according to ETA-14/0354 of »fischer PowerFast II« screws with an angle of $0^{\circ} \le \alpha \le 90^{\circ}$ shall be calculated according to equation (13).

$$F_{ax,\alpha,Rk} = n_{ef} \cdot k_{ax} \cdot f_{ax,\alpha|\alpha,k} \cdot d \cdot l_{ef} \cdot \left(\frac{\rho_k}{730}\right)^{0.8}$$
(13)

3.7.4.2 Withdrawal capacity *F*_{ax,Rk} for use in Cross-Laminated Timber

If there are no other technical specification (ETA or hEN) for Cross-Laminated Timber (CLT), the withdrawal capacity for screws can be calculated as following.

Screws in the plane surface

The withdrawal capacity for screws with $d \ge 6$ mm in the plane surface of CLT-elements should be assumed as for solid timber according to equation (10) based on a characteristic density of equation (14), if there are no other specifications are given. For not edge-bonded lamellas, equation (10) is only valid for screws with an outer diameter of $d \ge 5,0$ mm. If necessary gaps between the single lamellas have to be considered.

$$\rho_k = \mathbf{l}, \mathbf{l} \cdot \rho_{lay,k} \tag{14}$$

With

 $\rho_{\text{lay},k}$ Lowest characteristic density of the lamellas in a layer of the CLT-element [kg/m³]

Screws in the narrow side

The withdrawal capacity for screws in the narrow side of CLT-elements should be assumed according to equation (15).

$$F_{ax,Rk} = 20 \cdot d^{0,8} \cdot l_{ef}^{0,9} \tag{15}$$

Screws in the narrow side should be driven perpendicular into the grain of the lamella. The penetration length has to be at least $3 \cdot d + l_{ef}$.

If it is guaranteed that the angle between the lamellas and the screw axis is $\geq 30^{\circ}$ the characteristic withdrawal capacity from equation (15) can be increased of about 25 %.

For screws penetrating more than one layer of Cross-Laminated Timber, the different layers may be considered proportionally.

3.7.4.3 Withdrawal capacity *F*_{ax,Rk} for use in Wood-Based Panels

Screws in the plane surface

The characteristic axial withdrawal capacity of »fischer PowerFast II« screws with an angle of $\alpha = 90|90$ in wood-based panels with a minimum thickness and/or a penetration depth of the threaded part of at least $4 \cdot d$ can be calculated according to equation (16) for applications in the plane surface.

$$F_{ax,\alpha,Rk} = n_{ef} \cdot f_{ax,90|90,k} \cdot d \cdot l_{ef}$$
(16)



Figure 3: PowerFast II in the plane surface

Where

 $f_{ax,90|90,k}$ Characteristic withdrawal parameter in the plane surface, shown in Table 6

»fischer PowerFast II« screws in the plane surface		
PowerFast II	OSB (EN .	300)
d= 3,0 mm	$f_{ax,90 90,k} =$	9,3 N/mm ²
d= 3,5 mm	$f_{ax,90 90,k} =$	9,0 N/mm ²
d= 4,0 mm	$f_{ax,90 90,k} =$	8,6 N/mm ²
d= 4,5 mm	$f_{ax,90 90,k} =$	8,3 N/mm ²
d= 5,0 mm	$f_{ax,90 90,k} =$	8,0 N/mm ²
d= 6,0 mm	$f_{ax,90 90,k} =$	7,1 N/mm ²
PowerFast II	Particleboar	rd (EN 312)
d= 3,0 mm	$f_{ax,90 90,k} =$	11,9 N/mm ²
d= 3,5 mm	$f_{ax,90 90,k} =$	11,1 N/mm ²
d= 4,0 mm	$f_{ax,90 90,k} =$	10,3 N/mm ²
d= 4,5 mm	$f_{ax,90 90,k} =$	9,5 N/mm ²
d= 5,0 mm	$f_{ax,90 90,k} =$	8,7 N/mm ²
d= 6,0 mm	$f_{ax,90 90,k} =$	7,1 N/mm ²
PowerFast II	Fibreboards	
	(EN 622-2,	EN 622-3)
d= 3,0 mm	$f_{ax,90 90,k} =$	13,2 N/mm ²
d= 3,5 mm	$f_{ax,90 90,k} =$	12,4 N/mm ²
d= 4,0 mm	$f_{ax,90 90,k} =$	11,6 N/mm ²
d= 4,5 mm	$f_{ax,90 90,k} =$	10,8 N/mm ²
d= 5,0 mm	$f_{ax,90 90,k} =$	10,0 N/mm ²
d= 6,0 mm	$f_{ax,90 90,k} =$	8,5 N/mm ²
PowerFast II	LVL (EN 1-	4374)
	$\rho_k \ge 480 \text{ kg}$	/m ³
d= 3,0 mm	$f_{ax,90 90,k} =$	16,0 N/mm ²
d= 3,5 mm	$f_{ax,90 90,k} =$	15,4 N/mm ²
d= 4,0 mm	$f_{ax,90 90,k} =$	14,7 N/mm ²
d= 4,5 mm	$f_{ax,90 90,k} =$	14,0 N/mm ²
d= 5,0 mm	$f_{ax,90 90,k} =$	13,3 N/mm ²
d= 6,0 mm	$f_{ax,90 90,k} =$	12,0 N/mm ²

Table 6: Characteristic withdrawal parameters of»fischer PowerFast II« screws in the plane surface

Screws in the narrow side

The characteristic axial withdrawal capacity of »fischer PowerFast II« screws for pre-drilled applications in the edge surface with an angle $\alpha = 90|00$ in wood-based panels with a thickness of at least $5 \cdot d$ arranged in the center of the thickness of the panel with a penetration depth of the threaded part of the screws of at least $6 \cdot d$ can be calculated according to equation (17).

$$F_{ax,\alpha,Rk} = n_{ef} \cdot f_{ax,90|00,k} \cdot d \cdot l_{ef}$$
(17)
$$\alpha = 90|00$$

Figure 4: PowerFast II in the edge surface

Where

 $f_{ax,90|00,k}$ Characteristic withdrawal parameter in the edge surface, shown in Table 7

Table 7: Characteristic withdrawal parameters of
»fischer PowerFast II« screws in the edge surface

»fischer PowerFast II« screws in the edge surface			
PowerFast II	OSB (EN	300)	
d= 4,0 mm	$f_{ax,90 00,k} =$	6,0 N/mm ²	
d= 4,5 mm	$f_{ax,90 00,k} =$	5,8 N/mm ²	
d= 5,0 mm	$f_{ax,90 00,k} =$	5,6 N/mm ²	
d= 6,0 mm	$f_{ax,90 00,k} =$	5,1 N/mm ²	
PowerFast II	Particleboa	rd (EN 312)	
d= 4,0 mm	$f_{ax,90 00,k} =$	5,6 N/mm ²	
d= 4,5 mm	$f_{ax,90 00,k} =$	5,4 N/mm ²	
d= 5,0 mm	$f_{ax,90 00,k} =$	5,2 N/mm ²	
d= 6,0 mm	$f_{ax,90 00,k} =$	4,7 N/mm ²	
PowerFast II	Fibreboards	5	
	(EN 622-2,	EN 622-3)	
d= 4,0 mm	$f_{ax,90 00,k} =$	7,0 N/mm ²	
d= 4,5 mm	$f_{ax,90 00,k} =$	6,5 N/mm ²	
d= 5,0 mm	$f_{ax,90 00,k} =$	6,0 N/mm ²	
d= 6,0 mm	$f_{ax,90 00,k} =$	5,1 N/mm ²	
PowerFast II	LVL (EN 1	4374)	
	$\rho_k \ge 480 \text{ kg}$	/m ³	
d= 4,0 mm	$f_{ax,90 00,k} =$	9,2 N/mm ²	
d= 4,5 mm	$f_{ax,90 00,k} =$	8,8 N/mm ²	
d= 5,0 mm	$f_{ax,90 00,k} =$	8,4 N/mm ²	
d= 6,0 mm	$f_{ax,90 00,k} =$	7,5 N/mm ²	

3.7.4.4 Effective number of screws *n*_{ef}

For axially loaded screws in tension, where the external force is parallel to the screw axis, the rules in EN 1995-1-1, 8.7.2 (8) should be applied.

$$n_{ef} = n^{0.9}$$
 (18)

For inclined screws in timber-to-timber or steel-totimber shear connections, where the screws are arranged under an angle $30^{\circ} \le \alpha \le 60^{\circ}$ between the shear plane and the screw axis, the effective number of screws n_{ef} should be determined with the equation below.

$$n_{ef} = \max \begin{cases} n^{0.9} \\ 0.9 \cdot n \end{cases}$$
(19)

With

n Number of (inclined/cross pairs) screws in a row parallel to the grain direction

For screws as compression reinforcement or inclined screws as fasteners in mechanically jointed beams or columns $n_{ef} = n$.

3.7.5 Head pull-through capacity *f*_{head,k}

3.7.5.1 Head pull-through capacity *f_{head,k}* for use in Solid Timber (EN 338, EN 15497), Glued-Laminated Timber (EN 14080) and Laminated Veneer Lumber according to (ETA-14/0354)

The characteristic head pull-through capacity of »fischer PowerFast II« screws in solid timber can be calculate as following.

$$F_{head,Rk} = n_{ef} \cdot f_{head,k} \cdot d_h^2 \cdot \left(\frac{\rho_k}{350}\right)^{0.8}$$
(20)

For timber elements with a thickness of at least 20 mm, the characteristic value of the head pull-through parameter $f_{head,k}$ can be taken into account as following.

Table 8: Head pull-through capacities in Solid Timber, GLT, CLT and LVL

Solid Timber, GET, CET did EFE			
Countersunk and Raised Countersunk,			
see Annex A1 and A2			
d= 3,0 mm	d _h = 6,0 mm	fhead,k=19,0 N/mm ²	
d= 3,5 mm	d _h = 7,0 mm	fhead,k=16,3 N/mm ²	
d= 4,0 mm	d _h = 8,0 mm	fhead,k=15,0 N/mm ²	
d= 4,5 mm	d _h = 8,8 mm	$f_{head,k}$ =14,2 N/mm ²	
d= 5,0 mm	d _h = 9,8 mm	$f_{head,k}$ =13,4 N/mm ²	
d= 6,0 mm	$d_h=11,8mm$	$f_{head,k}$ =13,0 N/mm ²	
Washer head, so	ee Annex A4		
d= 5,0 mm	d _h =11,0mm	$f_{head,k} = 20,0 \text{ N/mm}^2$	
d= 6,0 mm	d _h =13,5mm	$f_{head,k}$ = 15,5 N/mm ²	
Step Countersunk head, see Annex A5			
d= 5,0 mm	d _h =11,0mm	$f_{head,k}$ = 19,5 N/mm ²	
d= 6,0 mm	d _h =13,5mm	$f_{head,k} = 15,0 \text{ N/mm}^2$	
Screw with clamping effect, see Annex A6			
d= 3,5 mm	d= 7,0 mm	$f_{head,k} \cdot d_h^2 = 1220 \text{ N}$	
d= 4,0 mm	d= 8,0 mm	$f_{head,k} \cdot d_h^2 = 1485 \text{ N}$	
d= 4,5 mm	d= 9,0 mm	$f_{head,k} \cdot d_h^2 = 1750 \text{ N}$	

3.7.5.2 Head pull-through capacity *f*_{head,k} for use in Wood-Based Panels

For the following wood-based panels described in Chapter 1 with a thickness of more than 20 mm the head pull-through parameter can constitute with

$$f_{head,k} = 10 \text{ N/mm}^2 \tag{21}$$

For wood-based panels with a thickness between 12 mm and 20 mm the characteristic value of the head pull-through parameter can be calculated with

$$f_{head,k} = 8 \text{ N/mm}^2 \tag{22}$$

For wood-based panels with a thickness of less than 12 mm the characteristic head pull-through capacity

shall be calculated with $f_{head,k}=8 N/mm^2$ with a limit of 400 N complying with a minimum thickness of the wood based panels of 1,2 ·d. In addition, to apply the minimum thickness of *Table 9*.

Table 9: Minimum thickness of Wood-Based Panels
be fixed on the side of the screw head

	Min.
Wood-based panel	thickness
	[mm]
Plywood	6
Oriented Strand board OSB	8
Solid wood panels	12
Particleboards	8
Cement bonded particle boards	8
Fibreboards (hard boards and	6
medium boards)	0
Gypsum fibre and Plasterboards	12

3.7.5.3 Head pull/push-through capacity of the FAFS-Clip of adjustable frame screw

The screws with the FAFS- Clip may be arranged under an angle of about 90° .

The load bearing capacities given in this section are valid for a quality of the battens of at least C20 $(\rho_k \ge 330 \text{ kg/m}^3)$.

The characteristic head pull-through capacity in softwood of the FAFS–Clip of adjustable frame screw can be calculated for tension loads onto the screws with

$$F_{FAFS,t,Rk} = 2200 \text{ N} \tag{23}$$

and for compression loads (push-through capacity) onto the screws with

$$F_{FAFS,c,Rk} = 1290 \text{ N}$$
 (24)

3.7.6 Tensile capacity *f*_{tens,k}

The characteristic tensile capacity $f_{tens,k}$ of »fischer PowerFast II« screws depending on the outer diameter is given below.

Table 10: Tensile capacity			
PowerFast II			
d= 3,0 mm	$f_{tens,k} =$	3,2 kN	
d= 3,5 mm	$f_{tens,k} =$	4,1 kN	
d= 4,0 mm	$f_{tens,k} =$	5,2 kN	
d= 4,5 mm	$f_{tens,k} =$	6,3 kN	
d= 5,0 mm	$f_{tens,k} =$	8,9 kN	
d= 6,0 mm	$f_{tens,k} =$	13,1 kN	

The tear-off capacity of the screw head is greater than the tensile capacity of the screw.

3.7.7 Compression capacity

The design compressive capacity $F_{ax,Rd}$ of »fischer PowerFast II« screws with full thread along the length embedded in timber shall be calculated as following.

$$F_{ax,Rd} = \min \begin{cases} F_{ax,Rd} \\ F_{ki,Rd} \end{cases}$$
(25)

Where

 $F_{ax,Rd}$ According to equation (10) $F_{ki,Rd}$ According to equation (26)

$$F_{ki,Rd} = \kappa_c \cdot N_{pl,d} \tag{26}$$

With

$$\kappa_c = 1$$
 for $\overline{\lambda} \le 0, 2$

$$\kappa_c = \frac{1}{k + \sqrt{k^2 - \overline{\lambda}^2}} \quad \text{for } \overline{\lambda} > 0, 2 \quad (27)$$

and

$$k = 0,5 \cdot \left[1 + 0,49 \cdot \left(\overline{\lambda} - 0,2\right) + \overline{\lambda}^2\right] \quad (28)$$

The relative slenderness ratio shall be calculated with

$$\overline{\lambda} = \sqrt{\frac{N_{pl,k}}{N_{ki,k}}}$$
(29)

With the characteristic value for the axial capacity in case of plastic analysis referred to the outer thread diameter. Yield strength $f_{y,k}$ see equation (8)..

$$N_{pl,k} = \frac{(0,7 \cdot d)^2 \cdot \pi}{4} \cdot f_{y,k}$$
(30)

And the characteristic ideal elastic buckling load

$$N_{ki,k} = \sqrt{c_h \cdot E_s \cdot I_s} \tag{31}$$

With the

Elastic foundation of the screw:

$$c_h = (0,19+0,0084 \cdot d) \cdot \rho_k \cdot \left(\frac{\alpha}{180^\circ} + 0,5\right)$$
 (32)

Modulus of elasticity:

$$E_s = 210.000 \text{ N/mm}^2$$
 (33)

Second moment of area:

$$I_s = \frac{\pi \cdot (0, 7 \cdot d)^4}{64}$$
(34)

Note: The compressive capacity must be modified for $f_{ax,d}$ with the factors k_{mod} and γ_M for timber according to EN 1995-1-1 while $N_{pl,d}$ the partial-factor $\gamma_{M,1}$ for steel buckling according to EN 1993-1-1 and/or national standards respectively have to be considered.

3.7.8 Combined laterally and axially loaded screws

For connections subjected to a combination of axial and lateral loads, the following expression has to be considered according to equation (35).

$$\left(\frac{F_{ax,Ed}}{F_{ax,Rd}}\right)^2 + \left(\frac{F_{v,Ed}}{F_{v,Rd}}\right)^2 \le 1$$
(35)

With

- $F_{ax,Ed}$ Axial design action [N]
- $F_{v,Ed}$ Lateral design action [N]
- $F_{ax,Rd}$ Design load-carrying capacity of an axially loaded screw [N]
- $F_{v,Rd}$ Design load-carrying capacity of a laterally loaded screw [N]

3.7.9 Slip modulus in the serviceability limit state

Laterally loaded screws

For laterally loaded »fischer PowerFast II« screws, the slip modulus, pre-drilled or non-pre-drilled, for the serviceability limit state (SLS) should be calculated according to EN 1995-1-1 independent of the load grain-direction angle α with equation (36).

$$K_{v,ser} = k_{st} \cdot k_{sp} \cdot C_{v,ser}$$
(36)

With

 $k_{st} = \begin{cases} 1 & \text{for timber-timber connections} \\ 2 & \text{for steel-timber connections} \end{cases}$

 k_{sp} Number of shear planes



Figure 5: Definition of the shear plane k_{sp}

Where

 ρ_m Mean timber density [kg/m³]

With

 $C_{v,ser}$ Slip modulus in SLS, Table 11[N/mm]

_	Table 11: Slip modules for laterally load	ed screws
	Matarial	C

Material	$C_{v,ser}$
	[N/mm]
Solid Timber	
Glued-Laminated Timber	a ^{1,5} d
Softwood and	$\frac{\rho_m^{1,5} \cdot d}{23}$
Hardwood	23
(EN 338, EN 15497, EN 14080)	
OSB	
t > 5 mm	$6,8\cdot ho_m\cdot d^{-0,4}$
(EN 300)	-
Plywood	
t > 4 mm	740
(EN 314-2)	
Fibreboards	
t > 3 mm	$9 \cdot \rho_m \cdot d^{-0,9}$
(EN 622-2, EN 622-3)	-
Particleboards	
t > 5 mm	$3 \cdot \rho_m \cdot d^{-0,4}$
(EN 312)	
Gypsum plasterboards	
t≥9 mm	$6700 \cdot d^{-087}$
(EN 520)	
Gypsum boards with fibrous	
reinforcement	14 F0.7
t≥9 mm	$1, 4 \cdot \rho_m \cdot d^{-0,7}$
(EN 15283-2)	
LVĹ	- 1.5 -1
Soft- and Hardwood	$\underline{\rho_m^{1,5} \cdot d}$
(EN 14374)	20
	· · · · · · · · · · · · · · · · · · ·

Axially loaded screws

For axially loaded screws the slip modulus for the serviceability limit state (SLS) can be calculated according to equation (37).

$$K_{ax,ser} = C_{ax,ser} \tag{37}$$

With

- *d* Outer thread diameter [mm]
- *l*_{ef} Penetration length of the threaded part in [mm]
- *C_{v,ser}* Slip modulus in SLS, Table 12 [N/mm]

<i>Table 12: S</i>	Slip	modules	for axially	loaded screws,
		1 1	C	

Table 12: Sup modules for axially loaded screws, only plane surfaces		
Material	$C_{ax,ser}$ [N/mm]	
Softwood		
$\rho_k \ge 350 \text{ kg/m}^3$	22. 1.1.	
independend of the	$32 \cdot d \cdot l_{ef}$	
angle α		
Hardwood		
$\rho_k \ge 510 \text{ kg/m}^3$	20.1.1	
independend of the	$38 \cdot d \cdot l_{ef}$	
angle α		
OSB		
t > 5 mm	$10 \cdot d \cdot l_{ef}$	
(EN 300)		
Fibreboards		
t > 3 mm	15·d·l _{ef}	
(EN 622-2, EN 622-3)		
Particleboards		
t > 5 mm	$10 \cdot d \cdot l_{ef}$	
(EN 312)		
LVL (EN 14374)		
Soft- and Hardwood		
$\rho_k \ge 480 \text{ kg/m}^3$	$28 \cdot d \cdot l_{ef}$	
α=90 90		
see Figure 2		

3.7.10 Slip modulus in the ultimate limit state

To consider the slip modulus K_u in the ultimate limit state (ULS) K_{ser} has to be reduced for both directions (laterally and axially) according to EN 1995-1-1 with

$$K_u = 2/3 \cdot K_{ser} \tag{38}$$

3.7.11 Minimum timber cross section, end- and edge distances

For structural timber members, minimum spacing and distances for screws in pre-drilled holes are given in EN 1995-1-1 clause 8.3.1.2 and table 8.2 as for nails in pre-drilled holes. Here, the outer thread diameter d must be considered.

Minimum thickness for structural members is in general t = 24 mm.

The FAFS-Clips may only be used in solid timber made of softwood. For the FAFS- Clip the minimum distances a1 and the minimum distances to the end grain in softwood have to be 60 mm for predrilled applications and 120 mm for non-predrilled applications.

The minimum cross section for predrilled and nonpredrilled applications in softwood has to be at least $30 \times 50 \text{ mm}^2$, minimum width of 50 mm and $a_{4,t} \ge 25$ *mm*. Predrilling is allowed with a diameter of 5 mm.

A combination of predrilled and non- predrilled holes for the screws with the FAFS- Clip is permitted, e.g., if only the hole for the screw with FAFS- Clip positioned close the end grain is predrilled in the batten and a distance to the end grain of 60 mm is considered. The following screws in the batten do not have to be pre- drilled, but a distance between the screws with the FAFS- Clip of 120 mm then has to be considered.

3.7.11.1 Solid Timber (EN 338, EN 15497) and Glued-Laminated Timber (EN 14080)

Minimum distances and spacing for laterally loaded »fischer PowerFast II« screws in non-pre-drilled holes in members of solid timber, glued-laminated timber or similar glued products with a minimum thickness $t = 12 \cdot d$ and a minimum width of 60 mm, should be chosen with Table 14

Table 13: Head shapes, see Table 14 to Table 17

¹⁾ Head shapes	Description
A	Screws with countersunk, step countersunk according to Annex A1, A2 and A6
	Screws with pan head and washer head according to Annex A3, A4 and A5
STEEL PLATE	Screws to fix steel plates on the head side according to Annex A1, A2, A3, A4, A5

Table 14: Laterally loaded screws: Minimum end- and edge distances for solid timber and glued-laminated timber products with a maximum gross density of 480 kg/m³ for non pre-drilled screws shown in Annex A1 to A5



Notations	
<i>a</i> 1	Spacing a_1 parallel to the grain of solid timber
a_2	Spacing a_2 perpendicular to the grain of solid timber
<i>a</i> _{3,c}	Distance $a_{3,c}$ from centre of the screw- part in timber to the unloaded end grain of solid timber
<i>a</i> _{3,t}	Distance $a_{4,c}$ from centre of the screw- part in timber to the loaded end grain of solid timber
<i>a</i> _{4,c}	Distance $a_{4,c}$ from centre of the screw- part in timber to the unloaded edge of solid timber
<i>a</i> _{4,t}	Distance $a_{4,t}$ from centre of the screw- part in timber to the loaded edge of solid timber

¹⁾ Head shape see Table 13

Minimum distances and spacing for exclusively axially loaded »fischer PowerFast II« screws in nonpredrilled holes in members of solid timber (softwood and hardwood), glued laminated timber or similar glued products (softwood and hardwood) with a minimum thickness $t = 12 \cdot d$ and a minimum width of 60 mm, whichever is the greater, may be taken as:

 Table 15: Axially loaded screws: Minimum end- and
 edge distances for Solid Timber and
 Glued-Laminated Timber products



¹⁾ Head shape see Table 13

Spacing a₂ perpendicular to the grain may be reduced from $5 \cdot d$ to $2, 5 \cdot d$, if the condition $a_1 \cdot a_2 \ge 25 \cdot d^2$ is fulfilled. For Douglas fir members minimum spacing and distances parallel to the grain shall be increased by 50 %.

Minimum distances from the unloaded edge perpendicular to the grain may be reduced to $3 \cdot d$ also for timber thickness $t < 5 \cdot d$, if the spacing parallel to the grain and the end distance is at least $25 \cdot d$.

3.7.11.2 Cross-Laminated Timber

Unless specified otherwise in the technical specification (ETA or hEN) of Cross-Laminated Timber, minimum distances and spacing for screws in the plane surface of Cross-Laminated timber members with a minimum thickness $t = 10 \cdot d$ may be taken as shown in Table 16 and Table 17.

Unless specified otherwise in the technical specification (ETA or hEN) of Cross-laminated timber, minimum distances and spacing for screws in the edge surface of Cross-laminated timber members with a minimum thickness $t = 10 \cdot d$ and a minimum penetration depth perpendicular to the edge surface of $10 \cdot d$ may be considered.

Table 16: Laterally and axially loaded screws: Minimum end- and edge distances for Cross-Laminated Timber in the plane surface

- Cross-Laminated Timber
- Screws in the plane surface





¹⁾ Head shape see Table 13

Table 17: Laterally and axially loaded screws: Minimum endand edge distances for Cross-Laminated Timber in the edge surface

Cross-Laminated Timber

- Screws in the edge surface



Head	N	linimur	n spacir	ng and di	stances				
shape ¹⁾	a_1	a_2	<i>a</i> _{3,c}	<i>a</i> _{3,t}	<i>a</i> _{4,c}	<i>a</i> _{4,t}			
	10·d	3·d	7·d	12·d	5·d	5·d			
Î	10·d	3·d	7·d	12·d	5·d	5·d			
STEEL PLATE	7·d	3·d	7·d	12·d	5·d	5·d			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$									
$F \xrightarrow{i} f \xrightarrow{i} $									

Notations

a_1	Spacing a_1 parallel to the plane direction								
<i>u</i> ₁	of the CLT-panel								
a	Spacing a_2 perpendicular to plane								
a_2	direction of the CLT-panel								
	Distance $a_{3,c}$ from centre of the screw-								
$a_{3,c}$	part in timber to the unloaded edge in								
	plane direction of the CLT-panel								
	Distance $a_{3,t}$ from centre of the screw-								
$a_{3,t}$	part in timber to the loaded edge in plane								
	direction of the CLT-panel								
	Distance $a_{4,c}$ from centre of the screw-								
a	part in timber to the unloaded edge								
$a_{4,c}$	perpendicular to the plane direction of								
	the CLT-panel								
	Distance $a_{4,t}$ from centre of the screw-								
	part in timber to the loaded edge								
$a_{4,t}$	perpendicular to the plane direction of								
	the CLT-panel								
1) 11 1 1	T 11 12								

¹⁾ Head shape see Table 13

For a crossed screw couple, the minimum spacing between the crossing screws should be at least $1,5 \cdot d$.

3.8 Durability against corrosion

3.8.1 Corrosion protection in Service Class 1 and 2

The »fischer PowerFast II« screws are produced from carbon steel. They are zinc-plated (e.g. yellow-zinced or blue-zinced), bonus-zinc-coated, burnished, nickel-plated or brass-plated. The mean thickness of the zinc-plated screws is min. 5 μ m.

3.9 General aspects related to the intended use of the product

The screws are manufactured in accordance with the provisions of the European Technical Assessment using the automated manufacturing process as identified during the inspection of the plant by the assessment body issuing the ETA and the notified body and laid down in the technical documentation. The installation shall be carried out in accordance with Eurocode 5 or an appropriate national code and in accordance with the instructions from fischerwerke GmbH & Co. KG.

4 Attestation and verification of constancy of performance (AVCP)

4.1 AVCP system

According to the decision 97/176/EC of the European Commission, as amended, the system(s) of assessment and verification of constancy of performance (see Annex V to Regulation (EU) No 305/2011) is 3.

Annex A: Product details and definitions Table A1: Screw sizes and material

	Pow	erFast	ll - Self	drilli	ng sc	rew -	Coun	tersur	nk hea	nd wit	h full	or pa	artial	threa	d
						ls ²⁾		- 1							
		Lindo	rhood	-		lgf									
Underhead milling pockets ¹															
	ů – ř														
			-ਰਿ		199	<u>EEEE</u>	AAT.	der 2	٦	(• * •)		60	2 •)		
				ĥ		4	lgp			Drive PZ	2	Driv	ve TX		
	¹⁾ optiona		Shank ribs ¹⁾ —					Core	emiller ¹⁾				Figure	not to cool	
	arbon												Figure	not to scale	8
• P	ossible	e surface t	treatments					lated, b	lue zinc-	plated 2	≥12µm,	bonus-z	inc-coa	ted, bur	nished,
nickel plated, brass plated Nominal diameter 3,0 3,5 4,0 4,5 5,0 6,0									· •						
INC	-	er thread of			,0 00		, 5 50		, 0 00		, 5 50		,0 10		,0 ,00
d		w. deviatio			,25),25		,30		,30		,30		, <u>00</u>),30
d1	Inne	er thread di	iameter	1,	95	2,	20	2,	50	2,	75	3,	25	3	,95
чı		w. deviatio			,18		,18		,20		,20		,20),20
dh		d diamete			00		00		00		80		80		,80
		w. deviation nk diamet			,50 25	-	,50 60		,60 90		,60 20		,60 70),60 ,30
ds		w. deviatio			,15		00 ,15		,15		,15),15		, <u>50</u>),15
h	Hea	id height			30		50		80		90	3,	40		,50
	Drive TX			1	0	10 20			20		0	20	25		30
		prive PZ	2)	<u> </u>	1	2		2		2		2		3	
		v length l	s ²⁾	Star	idard ti	nread le	ength	l _{gf} = ⊢ul	I thread	l _{gp} =	Partial	thread	I olera	ance: ±	2,03)
Nom lenç	gth	min	max	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}
20		l _s –1,05	l _s +1,05	16		16			10						
<u>2</u> 5 30		l _s −1,25 l _s −1,25	l _s +1,25 l _s +1,25	21 26	18 18	21 26	18 18	20 25	18 18	20 25	18	24			
35		ls –1,20	ls +1,20	31	24	31	24	30	24	30	24	29	24	28	
40		l₅ –1,50	l _s +1,50	36	28	36	28	35	28	35	28	34	28	33	28
45		l _s –1,50	l _s +1,50	41	30	41	30	40	30	40	30	39	30	38	30
50		ls -1,50	l _s +1,50			46	30	45	30	45	30	44	30	43	30
<u>55</u> 60		l _s –1,75	l _s +1,75					50 55	36 36	50 55	36 36	49 54	36 36	48 53	36 36
70		l _s –1,75	l _s +1,75 l _s +1,75					55	42	65	42	64	42	63	42
80		ls –1,75							45	75	45	74	45	73	45
90	0	ls -2,00	ls +2,00										54		54
10		ls –2,00	ls +2,00										60		60
11		ls -2,00	l _s +2,00										70		70
12		<u>l₅ –2,00</u> ps of 10m											70		70
130-		ls –3,00	ls +3,00												70
 Screws with partial thread > 60 mm l_s with shank ribs ²⁾ Other screw lengths with l_s min ≤ l_s ≤ l_s max and other thread lengths l_{gf} resp. l_{gp} ≥ 4xd up to max. standard thread lengths are allowed ³⁾ For 10mm ≤ l_{gf} resp., l_{gp} ≤ 18mm → tolerance ±1,5mm and for 18mm < l_{gf} resp. l_{gp} ≤ 30mm → tolerance ±1,7mm fischer PowerFast II 															
	Screw sizes and material														

Table A2: Screw sizes and material

Pov	werF	ast II -	Self-dri	lling s	screw	– Rais	sed co	ounter	sunk	head	with f	ull- or	partia	al thre	ad
						ls ²⁾									
		Lindonhoos		-		lgf									
		Underhead milling poc	kets ¹⁾								Tra	ade mark			
			g G												
			ਦ 🛓	1222	121	<i>\\\\</i>	RACKE				E)		60		
				/		-0-0-0-0	lgp			, P	Ì		S	/	
			1)	-/	-		t gp		1)	Drive	PZ		Drive T	Х	
¹⁾ optional	r.	Shank	ribs					Co	oremiller'				F	- igure not	to scale
		Steel											•	iguro not	
■ Po:															
No	mina	al diame	eter	3	,0	3	,5	4	,0	4	,5	5	,0	6	6,0
d		er thread o			00		50		00		50		10		,00
– –		w. deviatio),25 05		,25		,30 50		,30),30 25		0,30
d1		er thread di w. deviatio			95),18		20 ,18		50 ,20	2,	75 ,20		25),20		,95),20
├ ──┼		d diamete			00	-	00		00 00	±0 8,			<u>,20</u> 80		J,20 I,80
dh		w. deviatio	-		00),50		00 ,50		00 ,60		,60		00),60),60
4		nk diamet			25		60		90		20		70		,30
ds		w. deviatio	on),15		,15		,15		,15),15		0,15
h		d height			80		30	2,40			70		00		,60
		orive TX orive PZ			0 1	10 20			2 2	20 2		20 25 2		<u> </u>	
		v length l	2)		•	•	-	l _{gf} = Ful							-
Nomir		vienguri	s [_] ′	Star		lieaule	ngur j	lgt – Fui	linead	ו – נקף – ו 	artiar	lineau		ance. ± I	2,0°
lengt		min	max	ι _{gf}	l _{gp}	l _{gf}	l _{gp}	ι _{gf}	l _{gp}	l _{gf}	l _{gp}	ι _{gf}	l _{gp}	l _{gf}	l _{gp}
20		l _s –1,05	l _s +1,05	16	10	16	40		10						
25 30		ls −1,25 ls −1,25	l _s +1,25 l _s +1,25	21 26	18 18	21 26	18 18	20 25	18 18	20 25	18	24			_
35		ls –1,20	ls +1,20	31	24	31	24	30	24	30	24	29	24	28	
40		l _s –1,50	l _s +1,50	36	28	36	28	35	28	35	28	34	28	33	28
45		l _s –1,50	l _s +1,50	41	30	41	30	40	30	40	30	39	30	38	30
50			ls +1,50			46	30	45	30	45	30	44	30	43	30
55			l _s +1,75					50	36	50	36	49	36	48	36
60			l _s +1,75					55	36	55	36	54 64	36	53	36
70 80		ls –1,75 ls –1,75	ls +1,75 ls +1,75						42 45	65 75	42 45	64 74	42 45	63 73	42 45
90		$l_{s} = 1,73$ $l_{s} = 2,00$											54		54
100		l _s –2,00	l _s +2,00										60		60
110		l _s –2,00	l _s +2,00										70		70
120		l _s –2,00	l _s +2,00										70		70
i 130-30		ps of 10m l _s –3,00	m ls +3,00												70
130-30		ιs –3,00	is +3,00			<u> </u>		<u> </u>		<u> </u>		<u> </u>	Δ١١	sizes ir	-
²⁾ Othe lengt	er scre ths ar	ew lengths e allowed	al thread > s with l₅ mi o. l _{gp} ≤ 18 r	n ≤ ls ≤	l₅ max a	and othe	er thread	-					andard	thread	
			f	ischer	Powe	erFast	: 11					/	Annex	(A2	
			Sc	rew si	zes ar	nd mate	erial								

Table A3: Screw sizes and material

ls^{2} lgf lgf lgf lgg $Drive PZ$ $Drive PZ$ lgg $Drive PZ$ $Drive PZ$ lgg $Drive PZ$	Drive TX Figur	re not to scale d, burnished, 6,0 6,00							
Igr Igr Trade n Trade n Trade n Trade n Trade n Shank ribs ¹ Drive PZ Drive PZ <tr< th=""><th>Drive TX Figur Drive TX 5,0 5,10 ± 0,30 3,25 ± 0,20</th><th>d, burnished, 6,0</th></tr<>	Drive TX Figur Drive TX 5,0 5,10 ± 0,30 3,25 ± 0,20	d, burnished, 6,0							
Image: standard diameterImage: standard diameter3,03,54,04,5Image: standard diameter3,03,54,04,5Image: standard diameter3,03,54,04,50Image: standard diameter3,03,54,04,50Image: standard diameter3,03,504,004,50Image: standard diameter1,952,202,502,75Image: standard diameter1,952,202,502,80Image: standard diameter2,252,602,903,20Image: standard diameter2,302,502,802,80Image: standard diameter1,15±0,15±0,15±0,15Image: standard diameter1,23222Image: standard diameter1,20202020Image: standard diameter1,2322Image: standard diameter1,23	Drive TX Figur Drive TX 5,0 5,10 ± 0,30 3,25 ± 0,20	d, burnished, 6,0							
$ \begin{array}{ c c c c c c } \hline & \hline $	Figur onus-zinc-coated 5,0 5,10 ± 0,30 3,25 ± 0,20	d, burnished, 6,0							
Image: transmission of the systemImage: transmission of transmissio	Figur onus-zinc-coated 5,0 5,10 ± 0,30 3,25 ± 0,20	d, burnished, 6,0							
Drive P2 Shank ribs1* Carbon Steel • Possible surface treatments: yellow zinc-plated, blue zinc-plated, blue zinc-plated ≥12µm, bornickel plated, brass platedNominal diameter3,03,54,04,5dOuter thread diameter3,003,504,004,50dAllow. deviation $\pm 0,25$ $\pm 0,25$ $\pm 0,30$ $\pm 0,30$ d1Inner thread diameter1,952,202,502,75d1Allow. deviation $\pm 0,18$ $\pm 0,18$ $\pm 0,20$ $\pm 0,20$ dhHead diameter6,007,008,009,00dhAllow. deviation $\pm 0,50$ $\pm 0,50$ $\pm 0,60$ $\pm 0,60$ dsShank diameter2,252,602,903,20dsAllow. deviation $\pm 0,15$ $\pm 0,15$ $\pm 0,15$ $\pm 0,15$ hHead height2,302,502,802,80Drive TX1010202020Drive PZ1222Screw length l_s^{21} Standard thread length $ l_{gf}$ = Full thread $ l_{gp}$ =Partial thr	Figur onus-zinc-coated 5,0 5,10 ± 0,30 3,25 ± 0,20	d, burnished, 6,0							
1 	5,0 5,10 ± 0,30 3,25 ± 0,20	d, burnished, 6,0							
• Carbon Steel• Possible surface treatments: yellow zinc-plated, blue zinc-plated, blue zinc-plated ≥12µm, bonickel plated, brass platedNominal diameter3,03,54,04,5dOuter thread diameter3,003,504,004,50dAllow. deviation± 0,25± 0,25± 0,30± 0,30d1Inner thread diameter1,952,202,502,75d1Allow. deviation± 0,18± 0,18± 0,20± 0,20dhHead diameter6,007,008,009,00dhAllow. deviation± 0,50± 0,50± 0,60± 0,60dsShank diameter2,252,602,903,20dsAllow. deviation± 0,15± 0,15± 0,15± 0,15hHead height2,302,502,802,80Drive TX1010202020Drive PZ1222Screw length ls ² Standard thread lengthlgr = Full threadlgp =Partial thr	5,0 5,10 ± 0,30 3,25 ± 0,20	d, burnished, 6,0							
• Possible surface treatments: yellow zinc-plated, blue zinc-plated, blue zinc-plated ≥12µm, bonickel plated, brass platedNominal diameter3,03,54,04,5dOuter thread diameter3,003,504,004,50dAllow. deviation±0,25±0,25±0,30±0,30d1Inner thread diameter1,952,202,502,75d1Allow. deviation±0,18±0,18±0,20±0,20dhHead diameter6,007,008,009,00dhAllow. deviation±0,50±0,50±0,60±0,60dsShank diameter2,252,602,903,20dsAllow. deviation±0,15±0,15±0,15±0,15hHead height2,302,502,802,80Drive TX1010202020Drive PZ1222Screw length ls ²	5,0 5,10 ± 0,30 3,25 ± 0,20	6,0							
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	5,10 ± 0,30 3,25 ± 0,20								
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	± 0,30 3,25 ± 0,20	6,00							
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	3,25 ± 0,20	± 0,30							
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	± 0,20	<u>± 0,30</u> 3,95							
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	10.00	± 0,20							
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	± 0,60	12,00 ± 0,60							
Allow. deviation $\pm 0,15$ $\pm 0,15$ $\pm 0,15$ $\pm 0,15$ h Head height 2,30 2,50 2,80 2,80 Drive TX 10 10 20 20 20 Drive PZ 1 2 2 2 Screw length l_s^{2} Standard thread length l_{gf} = Full thread l_{gp} =Partial thr	3,70	4,30							
$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	± 0,15	± 0,15							
Drive PZ1222Screw length l_s^{2} Standard thread length l_{gf} = Full thread l_{gp} =Partial thr	3,40 20 25	3,40 30							
	2	3							
	ead Tolerand	ce: ± 2,0 ³⁾							
length min max l _{gf} l _{gp}	l _{gf} l _{gp}	l _{gf} l _{gp}							
	24								
		28							
		33 28 38 30							
		43 30							
		48 36							
		53 36 63 42							
		73 45							
90 ls -2,00 ls +2,00	54	54							
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	60 70	60 70							
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	70	70							
in steps of 10mm									
130-300 ls -3,00 ls +3,00	Δ ei-	70 zes in mm							
• Screws with partial thread > 60 mm l_s with shank ribs									
 ²⁾ Other screw lengths with l_s min ≤ l_s ≤ l_s max and other thread lengths l_{gf} resp. l_{gp} ≥ 4xd up to max. standard thread lengths are allowed ³⁾ For 10 mm ≤ l_{gf} resp.,l_{gp} ≤ 18 mm → tolerance ±1,5 mm and for 18 mm < l_{gf} resp. l_{gp} ≤ 30 mm → tolerance ±1,7 mm 									
fischer PowerFast II	Annex A	43							
Screw sizes and material	Screw sizes and material								

Table A4: Screw sizes and material

P					screw	/ – Wa	asher head with ful	I- or partial thread	
					ls ²⁾ lgf		-		
		5	S B	F. F. F. F.	h h h h	1111	10 510 (A)	Trade mark ¹⁾	
	Shan		-/	-	-0-0-0-0	lgp	Drive PZ	Drive TX	
¹⁾ optional ■ Carbon	Ctaal							Figure not to scale	
		reatments:			ated, blu brass pl		blated, blue zinc-plated ≥12	2µm, bonus-zinc-coated, burnished,	
	nal diame			,0		,0			
	ter thread on the thread of th		<u>5,</u> + 0	<u>10</u> ,30		00),30			
Inn	er thread di			, <u>50</u> 25		95	1		
	ow. deviatio		± 0	,20	± (),20]		
d.	ad diamete ow. deviatio			,00		,50			
Sh	ank diamet			,00 70		,00 30			
as Allo	ow. deviatio			,15	± (),15			
	ad height		3,0 20	00		10			
	Drive TX Drive PZ			25		30 3			
	w length l	s ²⁾				-	l _{af} = Full thread lap =Pa	rtial thread Tolerance: $\pm 2,0^{3)}$	
Nominal			_		Ι.			, - , -	
length	min	max	l _{gf}	l _{gp}	ι _{gf}	l _{gp}			
20	l _s –1,05	l _s +1,05							
25 30	l _s −1,25 l _s −1,25	ls +1,25 ls +1,25	24						
35	$l_s = 1,23$	l _s +1,20	29	24	28				
40	ls –1,50	ls +1,50	34	28	33	28			
45	l _s –1,50	l _s +1,50	39	30	38	30			
50 55	l _s –1,50 l _s –1,75		44 49	30 36	43 48	30 36			
60	l _s –1,75		54	36	53	36			
70	l _s –1,75		64	42	63	42			
80	ls –1,75		74	45	73	45			
<u>90</u> 100	l _s -2,00			54 60		54 60			
110	ls -2,00			70		70			
120	ls -2,00	ls +2,00		70		70			
	eps of 10m	1				70			
130-300	ls –3,00		60	المناب	hord	70	1	All sizes in mm	
²⁾ Other sc	with partian rew lengthare allowed	s with l₅ mi					d lengths l _{gf} resp. l _{gp} ≥ 4xd	up to max. standard thread	
³⁾ For 10 m	ım ≤ l _{gf} resp	o.,l _{gp} ≤ 18 n	nm → to	olerance	e ±1,5m	m and f	or 18 mm < l _{gf} resp. l _{gp} ≤ 30	Dmm → tolerance ±1,7 mm	
		fi	scher	Powe	erFast	: 11		Annex A4	
	Screw sizes and material								

Table A5: Screw sizes and material

PowerF		Self-dri			/ – Ste	ep Co	untersunk he	ad with	n full- or	partial thread
					ls ²⁾					
			-		lgf					
		ds						Λ	Trade mark ¹⁾	\mathbb{N}
	_			ᢣ᠋᠆ᠬ᠆ᠰ	<u>~~~~~</u> ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<u> </u>		(III)		T
	dh	, ∂		591	<u> </u>	<u>I BR</u>	a <u>c</u>			••••
	Charal	h	-/	-		lgp	Coremiller ¹⁾	Drive PZ		Drive TX
¹⁾ optional	Shank						Coremilier			Figure not to scale
CarbonPossible		reatments		zinc-pla plated, l			plated, blue zinc-pla	ted ≥12µr	n, bonus-z	inc-coated, burnished,
Nomina	al diame	eter		,0	1	,0				
	er thread o			10		00				
Inne	<u>w. deviatio</u> er thread di) <u>,30</u> 25) <u>,30</u> 95	1			
	w. deviatio id diamete),20 ,00		± 0,20 13,50				
	w. deviatio			,00 ,00		,50 ,00	1			
	lerhead dia nk diamet			40		50				
	w. deviatio			3,70 4,30 ± 0,15 ± 0,15						
	id height ive TX					20 80				
	Drive PZ			2		3				
	v length l	s ²⁾	Star	ndard th	nread le	ength	l _{gf} = Full thread l	_{gp} =Partia	al thread	Tolerance: $\pm 2,0^{3)}$
Nominal length	min	max	l _{gf}	lgp	lgf	l _{gp}				
20	l₅ –1,05	l₅ +1,05								
25	ls –1,25	ls +1,25	24							
30 35	l _s –1,25 l _s –1,50	l _s +1,25 l _s +1,50	24	24	28					
40	l _s –1,50	ls +1,50	34	28	33	28				
45 50	l _s –1,50 l _s –1,50	l _s +1,50 l _s +1,50	39 44	30 30	38 43	30 30	-			
55			49	36	48	36	-			
60 70	ls –1,75 ls –1,75	l _s +1,75 l _s +1,75	54 64	36 42	53 63	36 42	-			
80	l _s –1,75	l _s +1,75	74	45	73	45				
90 100	l _s –2,00 l _s –2,00	l _s +2,00 l _s +2,00		54 60		54 60	-			
110	ls –2,00	ls +2,00		70		70	1			
120 in ste	l₅ –2,00 ps of 10m	ls +2,00 m		70		70	4			
130-300	l _s –3,00	l _s +3,00				70	1			
²⁾ Other scr	ew lengths						d lengths l _{gf} resp. l _{gp}	, ≥ 4xd up	to max. st	All sizes in mm andard thread
lengths ar ³⁾ For 10 mr			ım → to	lerance	±1,5 m	m and f	or 18 mm < l _{gf} resp.	l _{gp} ≤ 30 n	$nm \rightarrow toler$	ance ±1,7 mm
		f	scher	Powe	erFast	:			A	Annex A5
		Sc	rew si	zes an	id mate	erial				

Table A6: Screw sizes and material

• Carbon Steel • Possible surface treatments: yellow zinc-plated, blue zinc-plated, blue zinc-plated ≥12µm, bonus-zinc-coated, burn nickel plated, brass plated • Nominal diameter 3,5 4,0 4,5 • Allow. deviation ± 0,25 ± 0,30 ± 0,30 • 1 Inner thread diameter 2,20 2,50 2,75 • 20 0uter thread diameter ± 0,18 ± 0,20 ± 0,20 • 20 et thread diameter 7,00 8,00 9,00 • Allow. deviation ± 0,50 ± 0,60 ± 0,60 • Allow. deviation ± 0,50 ± 0,15 ± 0,15 • Allow. deviation ± 0,50 2,80 3,20 • Allow. deviation ± 0,50 2,80 2,80 • Drive TX 10 20 20 20 • Drive PZ 2 2 2 2 • Screw length ls ² Standard thread length la = Double thread lgp =Main thread Tolerance: ± • Nominal min max lu lgp lu lgp 20 ls -1,25 ls +1,25 10 16 10,5 16	Powe	erFast I	l - Self-c	drillin	g scr	ew wi	th cla	mping	g effec	ct – parti	ial/underhead thread
Pigure not 1 Figure not 1 • Carbon Steel • Possible surface treatments: yellow zinc-plated, blue zinc-plated ≥12µm, bonus-zinc-coated, burn nickel plated, brass plated Norminal diameter 3.5 4.0 4.5 d Outer thread diameter 2.20 2.50 2.75 d1 Inner thread diameter 2.20 2.50 2.75 Allow. deviation ± 0.30 ± 0.30 ± 0.30 d2 Outer thread diameter 7.00 4.0.60 ± 0.30 Allow. deviation ± 0.50 ± 0.160 ± 0.01 d4 Allow. deviation ± 0.50 ± 0.160 ± 0.175 d2 Outer thread diameter 7.00 8.00 9.00 Head diameter 2.60 2.80 3.20 Drive PZ 2 2 2 2 Screw length k2 ³ Standard thread length k4 = Double thread log= =Main thread Tolerance; ± Nominal length min max lu lgp lu lgp 20 k = 1.05 k + 1.05 10 16 10.5 16 12 30 k = 1.		Underhead milling poc	d kets ¹⁾	5 	G	ls ²⁾	LAL Igp			Drive PZ	
Possible surface treatments: yellow zinc-plated, blue zinc-plated, blue zinc-plated ≥ 12µm, bonus-zinc-coated, bun inckel plated, brass plated. Nominal diameter 3,5 4,0 4,5 d Outer thread diameter 3,50 4,00 4,50 di Allow, deviation ± 0,25 ± 0,30 ± 0,30 di Allow, deviation ± 0,18 ± 0,20 ± 0,20 di Allow, deviation ± 0,30 ± 0,30 ± 0,30 di Allow, deviation ± 0,18 ± 0,20 ± 0,30 di Allow, deviation ± 0,10 ± 0,30 ± 0,30 di Allow, deviation ± 0,15 ± 0,160 ± 0,60 di Allow, deviation ± 0,15 ± 0,15 ± 0,15 monov deviation ± 0,15 ± 0,15 ± 0,15 ± 0,15 brive PZ 2 2 2 2 2 Drive PZ 2 2 2 2 2 2 Screw length ls ¹⁰ 10 10 10 10 10 10 10 10 a0 L-1,25		Steel						C(bremilier		Figure not to scale
d Outer thread diameter 3.50 4.00 4.50 Allow, deviation ± 0.25 ± 0.30 ± 0.30 d1 Inner thread diameter 2.20 2.75 Allow, deviation ± 0.18 ± 0.20 ± 0.20 d2 Allow, deviation ± 0.30 ± 0.30 ± 0.30 dh Head diameter 7.00 8.00 9.00 dk Mick, deviation ± 0.50 ± 0.60 ± 0.60 dk Shank diameter 2.60 2.90 3.20 Allow, deviation ± 0.15 ± 0.15 ± 0.15 h Head height 2.50 2.80 2.80 Drive TX 10 20 20 20 Screw length k² Standard thread length k₂ = Double thread gp = Main thread Tolerance; ± Nominal min max lu lgp lu lgp lu lgp 20 k -1.05 k +1.05 10 16 10.5 16 12 12 30 k -1.50 k +1.50 10 24<			reatments:					lated, b	lue zinc-	plated ≥12	um, bonus-zinc-coated, burnished,
a Allow. deviation ± 0.25 ± 0.30 ± 0.30 d1 Inner thread diameter 2.20 2.50 2.75 Allow. deviation ± 0.18 ± 0.20 ± 0.20 d2 Outer thread diameter 4.00 4.50 5.00 da Head diameter 7.00 8.00 9.00 da Head diameter 7.00 8.00 9.00 Allow. deviation ± 0.15 ± 0.15 ± 0.15 b Head height 2.50 2.80 2.80 Drive PZ 2 2 2 2 2 20 16 -1.05 10 10 10 10 10 10 21 1.0.5 10 24 10.5 24 12 12 30 1.0.5 10 24 10.5 30 12 30 10 1	Nomina	al diame	eter	3	,5	· · · ·		4	,5		
Allow. deviation ± 0, 20 ± 0, 30 ± 0, 30 ± 0, 30 d1 Inter thread diameter 2, 20 2, 250 2, 75 Allow. deviation ± 0, 18 ± 0, 20 ± 0, 20 d2 Allow. deviation ± 0, 30 ± 0, 30 ± 0, 30 dh Head diameter 7, 00 8, 00 9, 00 d1 Head diameter 7, 00 ± 0, 60 ± 0, 60 d2 Allow. deviation ± 0, 50 ± 0, 60 ± 0, 60 d3 Hank diameter 2, 60 2, 90 3, 20 Drive TX 10 20 20 20 20 Drive PZ 2 2 2 2 2 Standard thread length d= couble thread lgp = Main thread Tolerance: ± Nominal gp = Main thread Tolerance: ± Nominal length min max lu lgp lu lgp 20 L -1,25 L +1,25 L L lgp lu lgp 30 L +1,25 10 16 10,5 24 12 lgt lgt <th></th> <td></td>											
01 Allow. deviation ± 0,18 ± 0,20 ± 0,20 02 Outer thread diameter 4,00 4,50 5,00 42 Allow. deviation ± 0,30 ± 0,30 ± 0,30 46 Head diameter 7,00 8,00 9,00 Allow. deviation ± 0,50 ± 0,60 ± 0,60 41 Allow. deviation ± 0,15 ± 0,15 ± 0,15 10 Head height 2,50 2,80 2,80 Drive PZ 2 2 2 2 Screw length L ² Standard thread length La = Double thread Lap =Main thread Tolerance: ± Nominal length min max Lu Lgp Lu Lgp 20 La = 1,05 La + 1,25 L L L 30 La = -1,50 La + 1,50 10 16 10,5 16 12 33 La = -1,50 La + 1,50 10 24 10,5 24 12 44 La = -1,50 La + 1,50 10 24 10,5 24 12 50	Allo										
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 ²⁾ Other screw lengths with l_s min ≤ l_s ≤ l_s max and other thread lengths l_{gp} ≥ 4xd up to max. standard thread lengths ar allowed ³⁾ For 10 mm ≤ l_d resp.,l_{gp} ≤ 18 mm → tolerance ±1,5 mm and for 18 mm < l_d resp. l_{gp} ≤ 30mm → tolerance ±1,7 mm 	130-300	ls −3,00	ι _s +3,00								
fischer PowerFast II Annex A6	All sizes in mm ²⁾ Other screw lengths with $l_s min \le l_s \le l_s$ max and other thread lengths $l_{gp} \ge 4xd$ up to max. standard thread lengths are allowed										
			fi	ischer	Powe	erFast	II				Annex A6
Screw sizes and material			Sc	rew si	zes an	id mate	erial				

Table A7: FAFS-Clip size and material



Table A8: Washer sizes and material



Annex B: Application examples and design references Table B1: Fixing on-roof insulation













Table B1.3: Fixing of on-roof insulation

	Design of the battens	
The bending	g stresses of the battens are calculated with	
	$M_{Ed} = \frac{\left(F_{Ed} + F_{s,Ed}\right) \cdot l_{char}}{4}$	(41)
Where	·	
F _{Ed} F _{s,Ed} M _{Ed} I _{char}	Point loads perpendicular to the battens [N] Point loads perpendicular to the battens in the area of the set Design bending moment of the batten [Nmm] Characteristic length of the batten [mm] with $l_{char} = \sqrt[4]{\frac{4 \cdot EI}{W_{ef} \cdot K}}$, where EI Bending stiffness of the batten [Nmm ²] w_{ef} Effective width of the thermal insulation [mm] with $w_{ef} = w + t_{ti} / 2$, where w Minimum width of the batten or rafter [mm] t_{ti} Thickness of the thermal insulation [mm] K Bedding modulus [N/mm ³] The coefficient K may be calculated from the mode the thickness t_{ti} of the thermal insulation if the effective width w_{ef} of the batten or rafter, respectively. For further can width w_{ef} of the thermal insulation may be determ E_{ti} Modulus of elasticity of the thermal insulation	dulus of elasticity E_{ti} and ective width w_{ef} of the Due to the load is greater than the width alculations, the effective ined with $K = \frac{E_{ti}}{t_{ti}}$, where
The followir	t_{ti} Thickness of the thermal insulation [mm] ng conditions shall be satisfied:	
	$rac{\sigma_{\!\!m,Ed}}{f_{\!\!m,d}}\!\leq\!\!1$	(42)
Where		
$\sigma_{m,Ed} \ f_{m,d}$	Design value of the bending stress of the batten [N/mm²] Design value of the bending strength [N/mm²]	
Where $f_{v,d}$ A_{ef} V_{Ed} $ au_{Ed}$	$\frac{\tau_{Ed}}{f_{v,d}} = \frac{3 \cdot V_{Ed}}{2 \cdot A_{ef} \cdot f_{v,d}} \leq 1$ Design value of the shear strength of the batten [N/mm ²] Net cross section of the batten [mm ²] Design shear load onto the batten [N] with $V_{Ed} = \frac{F_{Ed} + F_{s,Ed}}{2}$ Design value of the shear stress of the batten [N/mm ²]	(43)
	fischer PowerFast II	Annex B1.3
	Fixing of on-roof insulation	

Design of the heat insulation							
The compressive stresses in the thermal insulation shall be calculated with	1						
$\sigma_{c,Ed} = \frac{1.5 \cdot F_{Ed} + F_{s,Ed}}{2 \cdot l_{char} \cdot w_{ef}}$	(44)						
Where							
F_{Ed} Point loads perpendicular to the battens $[N]$ $F_{s,Ed}$ Point loads perpendicular to the battens in the area of the second characteristic length of the batten $[mm]$ with $l_{char} = \sqrt[4]{\frac{4 \cdot EI}{w_{ef} \cdot K}}$, where EI Bending stiffness of the batten $[Nmm^2]$ w_{ef} Effective width of the thermal insulation $[mm]$ with $w_{ef} = w + t_{ii} / 2$, where w Minimum width of the batten or rafter $[mm]$ t_{ii} Thickness of the thermal insulation $[mm]$ K Bedding modulus $[N/mm^3]$ The coefficient K may be calculated from the mootthe thickness t_{ii} of the thermal insulation if the effective width w_{ef} is greater tobatten or rafter, respectively. For further calculated w_{ef} of the thermal insulation may be determined w E_{ii} Modulus of elasticity of the thermal insulation $[mm]$ $\sigma_{c,Ed}$	dulus of elasticity E_{ti} and ective width w_{ef} of the Due to the load extension han the width of the ons, the effective width $tith K = \frac{E_{ti}}{t_{ti}}$, where [N/mm ²] ulation						
Note: The design value of the compressive stress shall not be greater than stress at 10 % deformation calculated according to EN 826.	110 % of the compressive						
fischer PowerFast II	Annex B1.4						
Fixing of on-roof insulation							

Table B1.5: Fixing of on-roof insulation

Design of the screws

The screws are loaded predominantly axially. The axial tension force in the screw may be calculated from the shear loads of the roof

$$F_{ax,Ed} = \frac{R_{s,Ed}}{\cos \alpha_r} \le F_{ax,\alpha,Rd}$$
(45)

Where

$F_{ax,Ed}$	Design value of the axial tension forces onto the screw [N]
$F_{ax,\alpha,Rd}$	Design value of the withdrawal capacity of the screw [N]
$R_{s,Ed}$	Shear loads onto the screw [N]
α_r	Angle inclined screw (see figure B1.2) [°]

The load-carrying capacity of axially loaded screws is the minimum design value of the axial withdrawal capacity of the threaded part of the screw, the head pull-through capacity of the screw and the tensile capacity of the screw.

In order to limit the deformation of the screw head for heat insulation thicknesses over 200 mm or with compressive strength below 0,12 N/mm², respectively, the axial withdrawal capacity of the screws shall be reduced by the factors k_1 and k_2 .

$$F_{ax,\alpha,Rd} = \min\left\{k_{ax} \cdot f_{ax,d} \cdot d \cdot l_{ef} \cdot k_1 \cdot k_2 \cdot \left(\frac{\rho_k}{350}\right)^{0,8}, f_{head,d} \cdot d_h^{-2} \cdot \left(\frac{\rho_k}{350}\right)^{0,8}, f_{tens,d}\right\}$$
(46)

Where

$F_{ax, \alpha, Rd}$	Design value of the withdrawal capacity of the screw [N]
d d	Diameter of the screw [mm]
d_h	Head diameter of the screw [mm]
$f_{ax,d}$	Design value of the withdrawal parameter of the threaded part of the screw [N/mm²]
fhead,d	Design value of the head pull-through capacity of the screw [N/mm ²]
ftens,d	Design value of the tensile capacity of the screw [N]
k _{ax}	Coefficient according to equation (11)
k_1	min {1; 200 / t_{ii} } [-]
k_2	min {1; $\sigma_{10\%,Ed}$ / 0,12} [-], where
	$\sigma_{10\%,Ed}$ Compressive stress of the heat insulation at 10 % deformation [N/mm ²]
	<i>t_{ti}</i> Thickness of the thermal insulation [mm]
l _{ef}	Point side penetration length of the threaded part in the rafter with $l_{ef} \ge 40$ mm
α	Angle between grain and screw axis ($\alpha \ge 30^\circ$) [°]
$ ho_k$	Characteristic density of the timber element [kg/m³]

Note: If in the equation for $F_{ax,Rd}$ the factors k_1 and k_2 are considered, the deflection of the battens does not need to be considered. Alternatively to the battens, panels with a minimum thickness of 20 mm from plywood according to EN 636 or an ETA or national provisions that apply at the installation site, particle board according to EN 312 or an ETA or national provisions that apply at the installation site, oriented strand board according to EN 300 or an ETA or national provisions that apply at the installation site and solid wood panels according to EN 13353 or an ETA or national provisions that apply at the installation site or Cross- laminated Timber according to an ETA may be used.

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Fixing of on-roof insulation	

Table B1.6: Fixing of on-roof insulation

Thermal insulation material on rafters with parallel screws perpendicular to the roof plane

Alternative to the battens, panels with a minimum thickness of 20 mm from plywood according to EN 636, particleboard according to EN 312, oriented strand board OSB/3 and OSB/4 according to EN 300 or European Technical Assessment and solid wood panels according to EN 13353 may be used.

Characteristic load-carrying capacity of a screw loaded in shear:

$$F_{v,Rk} = min \begin{cases} f_{h,b,k} \cdot d \cdot t_{b} \\ f_{h,r,k} \cdot d \cdot t_{r} \\ \frac{f_{h,b,k} \cdot d \cdot \beta}{1+\beta} \cdot \left(\sqrt{4t_{ii}^{2} + (2+\frac{1}{\beta})t_{b}^{2} + (2+\beta)t_{r}^{2} + 4t_{ii}\left(t_{b} + t_{r}\right) + 2t_{b}t_{r}} - 2t_{ii} - t_{b} - t_{r}\right) + \frac{F_{ax,Rk}}{4} \\ 1,05 \cdot \frac{f_{h,b,k} \cdot d \cdot \beta}{\frac{1}{2} + \beta} \left(\sqrt{t_{ii}^{2} + t_{ii}t_{b} + \frac{t_{b}^{2}}{2}\left(1 + \frac{1}{\beta}\right) + \frac{M_{y,k}}{f_{h,b,k} \cdot d}\left(1 + \frac{2}{\beta}\right)} - t_{ii} - \frac{t_{b}}{2}\right) + \frac{F_{ax,Rk}}{4} \\ 1,05 \cdot \frac{f_{h,b,k} \cdot d \cdot \beta}{\frac{1}{2} + \beta} \left(\sqrt{t_{ii}^{2} + t_{ii}t_{r} + \frac{t_{r}^{2}}{2}\left(1 + \beta\right) + \frac{M_{y,k}}{f_{h,b,k} \cdot d}\left(2 + \frac{1}{\beta}\right)} - t_{ii} - \frac{t_{r}}{2}\right) + \frac{F_{ax,Rk}}{4} \\ 1,15 \cdot \frac{f_{h,b,k} \cdot d}{1+\beta} \left(\sqrt{\beta^{2}t_{ii}^{2} + 4 \cdot \beta\left(\beta + 1\right) \cdot \frac{M_{y,k}}{f_{h,b,k} \cdot d}} - \beta \cdot t_{ii}\right) + \frac{F_{ax,Rk}}{4} \end{cases}$$

$$(47)$$

Where

$F_{v,RK}$	Characteristic load-carrying capacity of a screw loaded in shear [N]
$M_{y,k}$	Characteristic yield moment of the screw [Nmm]
$F_{ax,Rk}$	The minimum characteristic load-carrying capacity of the axially loaded
	screws acc. to EN 1995-1-1 [N]
$f_{h,b,k}$	Characteristic embedment strength of the batten [N/mm ²]
$f_{h,r,k}$	Characteristic embedment strength of the rafter [N/mm ²]
d	Outer thread diameter [mm]
t_b	Batten thickness [mm]
t _r	The lower value of rafter thickness or screw penetration length [mm]
t_{ti}	Thickness of the thermal insulation [mm]
β	Coefficient of the embedment strength of the rafter to the batten [-]
•	

with
$$\beta = \frac{f_{h,r,k}}{f_{h,b,k}}$$

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Annex B1.6

Fixing of on-roof insulation

Table B2: FAFS-Clip



Table B2.1: FAFS-Clip

FAFS-Clip of adjustable frame screw

with

$$k = 0, 5 \cdot \left[1 + 0, 49 \cdot \left(\overline{\lambda} - 0, 2 \right) + \overline{\lambda}^2 \right]$$
(52)

The relative slenderness ratio shall be calculated with

$$\overline{\lambda} = \frac{4 \cdot L_{cr}}{\pi \cdot (0, 7 \cdot d)} \cdot \sqrt{\frac{f_{y,k}}{E_s}}$$
(53)

With the characteristic value for the axial capacity in case of plastic analysis referred to the diameter

$$N_{pl,k} = \frac{(0,7 \cdot d)^2 \cdot \pi}{4} \cdot f_{y,k}$$
(54)

For screws with a diameter of 5 mm, according to Annex A1

$$N_{pl,k} = 8710 \text{ N}$$
 (55)

And the buckling length L_{cr} on the side of the screw tip with a minimum penetration depth of $8 \cdot d$

$$L_{cr} = 0, 7 \cdot l_d \tag{56}$$

Where

d e E _s	Nominal diameter of the screw [mm] Effective distance (supporting points) between parallel arranged screws [m] Modulus of elasticity of the screw [N/mm²], see chapter 3.7.7
$F_{ax,Rd}$	Design withdrawal capacity of the screw in the structural timber element (2) [N], see chapter 3.7.4
$F_{FAFS,t,Rd}$	Design head pull-through capacity of the FAFS-Clip in timber part (1) for tension forces [N], see chapter 3.7.5.3
$F_{FAFS,c,Rd}$	Design head push-through capacity of the FAFS-Clip in timber part (1) for compression forces [N], see chapter 3.7.5.3
Lcr	Buckling length of the screw [mm]
l_d	Distance between (1) and (2) [mm]
$N_{pl,k}$	Characteristic axial capacity in case of plastic analysis [N]
$q_{Ed}^{(+)}$	Design load effecting tension loads on the installation element (1) [N/m]
$q_{Ed}^{(-)}$	Design load effecting compression loads on the installation element (1) [N/m]

Note: The compressive capacity must be modified for $f_{ax,d}$ with the factors k_{mod} and γ_M for timber according to EN 1995-1-1 while $N_{pl,d}$ the partial-factor $\gamma_{M,1}$ for steel buckling according to EN 1993-1-1 and/or national standards must be considered.

fischer PowerFast II

Annex B2.1

FAFS-Clip Applications

Table B3: Inclined Screws



Table B3.1: Inclined Screws


Table B4: Fire Design



With

$$a_{fi} = 1, 5 \cdot \beta_n \cdot (t_{req} - t_{d,fi})$$
(63)



Table B4.1: Fire Design

Fire Design according to EN 1995-1-2

The values for the design notional charring rate β_n under standard fire exposure are given below.

Table B4.1: Notional charring rate

Material	β _n [mm/min]
Softwood and beech	
Glued-Laminated Timber with a characteristic density of \geq 290 kg/m ³	0,70
Solid Timber with a characteristic density of \geq 290 kg/m ³	0,80
Hardwood	
Solid or Glued-Laminated hardwood with a characteristic density of \ge 290 kg/m ³	0,70
Solid or Glued-Laminated hardwood with a characteristic density of \ge 450 kg/m ³	0,55
LVL	
LVL with a characteristic density of \geq 480 kg/m ³	0,70

b) Protected connections



If the construction is protected by the addition of wood panelling, wood-based panels or gypsum plasterboards type *A* or *H* or other fire protection panels with a fire resistance in accordance to an European Technical Assessment, the time until start of charring should satisfy

$$t_{ch} \ge t_{req} - 0, 5 \cdot t_{d,fi}$$

(64)

fischer PowerFast II	Annex B4.1
Fire Design	

Table B4.2: Fire Design

Fire Design according to EN 1995-1-2

If the connection is protected by the addition of gypsum plasterboard type F, the time until start of charring should satisfy equation (65).

$$t_{ch} \ge t_{reg} - 1, 2 \cdot t_{d,fi}$$
 (65)

For connections where the screws are protected by glued-in timber plugs, the length of the plugs should be determined according to

$$a_{fi} = 1, 5 \cdot \beta_n \cdot (t_{req} - t_{d,fi}) \tag{66}$$

The fixings of the additional protection should prevent its premature failure. Additional protection provided by wood-based panels or gypsum plasterboards should remain in place until charring of the member starts ($t = t_{ch}$). Additional protection provided by gypsum plasterboards type *F* should remain in place during the required fire resistance period ($t = t_{req}$).

The following rules apply for the fixing of additional protections by screws:

- The distance between the screws should be not more than 100 mm along the board edges and not more than 300 mm for fastenings within the area of the boards
- The edge distance of fasteners should be equal or greater than *a_{fi}*, calculated using expression

$$a_{fi} = 1, 5 \cdot \beta_n \cdot (t_{req} - t_{d,fi}) \tag{67}$$

The penetration depth of the screws for fixing the additional protection made of wood, woodbased panels or gypsum plasterboards type A or H should be at least $6 \cdot d$.

For gypsum plasterboards type F, the penetration length into unburnt wood (that is beyond the char-line) should be at least 10 mm (see also EN 1995-1-2).

Where

- *a_{fi}* Extra thickness of member to improve the fire resistance [mm]
- *t_{req}* Required time of fire resistance [min]
- $t_{d,fi}$ Time of the fire resistance of the unprotected connection [min]
- β_n Notional charring rate [mm/min]

Annex B4.2

fischer PowerFast II

Fire Design

Appendix 39

Table B4.3: Fire Design



Fire Design

Appendix 40

Table B5: Screw-Gluing



- partial threaded screw
- (2) Bonded part
- (3) Glue joint
- Thickness of the gluing parts t_1, t_2
- aı Spacing of the screws parallel to the grain in a row
- Screw length
- Threaded length (Igp for partial-threaded screws)
- Head diameter
- Distance of the screw to the unloaded end grain

The shown applications for screw-bonding applies only for structures in serviceability class 1 and 2 according to EN 1995-1-1. The use of an adhesive with joint filling properties is necessary. If the joint thickness of a maximum of 0.3 mm can be ensured, adhesives according to EN 15425 and adhesives type I may also be used according to EN 301. The adhesive manufacturer's instructions must be fulfilled. Only »fischer PowerFast II« screws with washer or step countersunk heads (see Annex A4 and A5) with a nominal diameter $d \ge 5$ mm should be used.

ls

lgf

dh

a3,c

In the use of partial-threaded screws, no part of the thread should be in the bonded part. When using fully threaded screws, the glued part must be pre-drilled with a borehole of at least d + 1.0 mm. The upper side of the screw head or the washer, must be countersunk at least 2 mm from the surface of the glued part. The figure above shows the different options for installing the partial threaded screws of the assembling structural elements.

fischer PowerFast II

Annex B5

Screw -Gluing

Appendix 41

Table B5.1: Screw-Gluing

Screw-Gluing

The minimum spacing for connections with axially loaded screws must be observed. The maximum distance in the adhesive surface to the ends of the components must be $a_{3,c} \le 10 \cdot d$, and to the edges $a_{4,c} \le 5 \cdot d$. With a single-row screw connection, the rib width b_{rib} may not be larger than $d_h + 2 \cdot t_1$, otherwise a multi-row screw connection must be carried out.





- $a_{3,c}$ Distance to the unloaded end grain
 - Width of the beam web
- d_h Head diameter
- l_{gf} Threaded length (l_{gp} for partial-threaded screws)

t ₁	Thickness of the bonded pa	nel
----------------	----------------------------	-----

to the grain direction

Glue ioint

grain in a row

Screw length

Partial threaded screw with washer

Spacing of the screws parallel to the

Spacing of the screws perpendicular

Distance to the unloaded edge

Nominal diameter of the screw

Legend

(1) (3)

a₁

 a_2

a4,c

d

 I_s

fischer PowerFast II	Annex B5.1
Screw -Gluing	

a₁*

b_{rip}

Table B5.2: Screw-Gluing

Screw-Gluing

The surfaces of the bonded parts must be suitable for bonding and are in accordance to the requirements of the adhesive manufacturer. In general, the finishes need be sanded or smoothed planed and without coatings, dirt, dust and impurities.

The tolerance of the joint thickness of the assembling parts must fulfil the tolerances for

- Beam- and plate-shaped screw-gluing: max. 1 mm per 1 m
- Ribbed panels: max. 2 mm per 2 m

If several layers are glued together, each layer must be screwed-on separately. The screws must be arranged staggered (see also figure Annex B 5.1, right below), to apply enough pressure in all joints. In the intermediate layers, the screw heads should not protrude the surface of the intermediate layer.

Deformations and movements that lead to damages of the adhesive-joints have to be avoided. The screw parameters and distances depend on the thickness of the assembling parts, given in the table below.

Material bonded part	Thickness bonded part [mm]	Recommended nominal diameter [mm]	Min. nominal head diameter [mm]	Maximum scree Parallel to the grain direction of the outer layer [mm]	w spacings Perpendicular to the grain direction of the outer layer [mm]	Length of the threaded screw part in the structural part [mm]	Calculated compressive stress <i>Pcal,min</i> [N/mm ²]
Beam- and panel sha	aped screw-gluin	ig	1		1		
LVL of softwood, three-layered solid timber panel, OSB	12 ≤ t < 19	≥ 5 e.g Annex A4, A5	9,8	100	65	6∙d	
LVL beech		, -		100	100	8∙d	
Lamellas and one- layered solid timber panels		≥ 6	10,8	140	65	6∙d	0,10
LVL in spruce three-layered solid timber panel, OSB	19 ≤ t < 27	e.g Annex A1	Washer, e.g Annex A8	140	90	6∙d	
LVL beech			10,8	140	140	8∙d	
	fis	scher PowerF	ast II			Annex E	35.2
Screw -Gluing							

Table B5.2: Properties of the bonded parts, screw parameters and compressive stress

Table B5.3: Screw-Gluing

Screw-Gluing

As an alternative to the specifications in the table Annex B5.2, the maximum screw spacing can also be determined with the empirical equation (71).

$$a_{i,max} = 3,35 \cdot \sqrt[4]{E_{mean,i} \cdot I_{i,b=1}}$$
(71)

with *i* = 1 or 2

In addition, it must be proven that the calculated minimum compressive stress per screw is observed

$$\frac{F_{ax,Rd}}{a_1 \cdot a_2} \ge p_{cal,min} \tag{72}$$

Where

$a_{i,max}$	Maximum spacing of the screws in i-direction [mm]
$I_{i.b=l}$	Moment of inertia in i-direction for a width of 1 mm of the bonded part [mm ⁴]
$E_{mean,i}$	Modulus of elasticity in i-direction of the bonded part [N/mm ²]
$a_{i,max}$	Maximum spacing of the screws [mm]
$F_{ax,Rd}$	Design withdrawal strength of the screw [N]
$p_{cal,min}$	Minimum calculated compressive stress according to Annex B5.2

For the characteristic head pull-through parameter $f_{head,k}$ the following models can be used:

- Screws with glued parts made of solid timber and wood-based materials in softwood with

$$f_{head,k} = 14 \cdot d_h^{-0.14} \cdot \left(\frac{\rho_k}{\rho_a}\right)^{0.8}$$
(73)

- Screws with glued parts made of LVL in beech with

$$f_{head,k} = 25 \text{ N/mm}^2 \tag{74}$$

The decrease in the pressure until the adhesive hardens, can be taken into account in the calculation model with $k_{mod} = 1,0$ and $\gamma_M = 1,3$. Table in Annex B5.2 is based on these model assumptions. After the required bond strength has been reached, the screws can be unscrewed.





DÉCLARATION DES PERFORMANCES



DoP: 0118

pour vis fischer Power-Fast II (Vis à utiliser dans des constructions en bois) - FR

1. Code d'identification unique du type de produit : DoP: 0118

2. Usage(s) prévu(s): Vis pour utilisation dans les constructions bois porteuses ou pour fixation de systèmes d'isolation thermique sur chevrons

- 3. Fabricant: fischerwerke GmbH & Co. KG, Klaus-Fischer-Straße 1, 72178 Waldachtal, Allemagne
- 4. Mandataire: --
- 5. Système(s) d'évaluation et de vérification de la constance des performances: 3
- 6. Document d'évaluation européen: EAD 130118-01-0603
 - Évaluation technique européenne: ETA-19/0175; 2020-01-07

Organisme d'évaluation technique: ETA-Danmark A/S

7. Performance(s) déclarée(s):

Résistance mécanique et stabilité (BWR 1), sécurité d'utilisation et accessibilité (BWR 4)

- Dimensions: voir annexes, en particulier les Annexes 12, 13, 14
- Moment d'écoulement plastique caractéristique : voir annexe, en particulier l'Annexe 5
- Angle de flexion: voir annexe, en particulier l'Annexe 1
- Paramètre de résistance caractéristique à l'arrachement: voir annexes, en particulier les Annexes 5, 6, 7
- Paramètre de résistance caractéristique à la traversée de la tête de vis: voir annexe, en particulier l'Annexe 7
- Résistance caractéristique en traction: voir annexe, en particulier l'Annexe 3
- Limite d'élasticité caractéristique: voir annexe, en particulier l'Annexe 5
- Résistance caractéristique à la torsion: voir annexe, en particulier l'Annexe 3
- Couple de serrage: voir annexe, en particulier l'Annexe 3
- Entraxes et distances des vis ou tiges filetées et épaisseur minimum du matériau bois: voir annexes, en particulier les Annexes 8, 9, 22
- Module de glissement pour les vis et tiges filetées sollicitées principalement axialement: voir annexe, en particulier l'Annexe 8
- Résistance à la corrosion: voir annexes, en particulier les Annexes 1, 10, 12, 13, 14

Protection contre l'incendie (BWR 2)

Réaction au feu: Les vis satisfont les exigences pour la classe A 1

8. Documentation technique appropriée et/ou documentation technique spécifique: ---

Les performances du produit identifié ci-dessus sont conformes aux performances déclarées. Conformément au règlement (UE) no 305/2011, la présente déclaration des performances est établie sous la seule responsabilité du fabricant mentionné ci-dessus.

Signé pour le fabricant et en son nom par:

Thilo Pregartner, Dr.-Ing.

Wolfgang Hengesbach, Dipl.-Ing., Dipl.-Wirtsch.-Ing.

ppa. The Mx

Tumlingen, 2020-02-17

i.V. W. Kgelal

- Cette déclaration des performances a été émise en différentes langues. En cas de divergences d'interprétation, la version anglaise prévaut toujours.
- L'annexe contient des informations volontaires et complémentaires en langue anglaise dépassant les exigences légales (spécifiées en langage neutre).

II SPECIFIC PART OF THE EUROPEAN TECHNICAL ASSESSMENT

1 Technical description of product and intended use

Technical description of the product

"fischer Power-Fast II" screws are self-tapping screws to be used in timber structures. They shall be threaded over a part of the length or over the whole length. The screws shall be produced from carbon steel wire for nominal diameters between 3,0 mm and 6,0 mm. Where corrosion protection is required, the material or coating shall be declared in accordance with the relevant specification given in Annex A of EN 14592.

Geometry and Material

The nominal diameter d (outer thread diameter) of the screws shall not be less than 3,0 mm and shall not be greater than 6,0 mm.

The overall length l_s of the screws, shall not be less than 20 mm and shall not be greater than 300 mm. Dimensions see Annex A.

The ratio of inner thread diameter to outer thread diameter d_1/d ranges from 0,50 to 0,80.

The screws are threaded over a minimum length l_g of 4,0 \cdot d (i.e. $l_g \ge 4,0 \cdot$ d).

The thread pitch p (distance between two adjacent thread flanks) ranges from 0,50 ·d to 0,85 ·d.

No breaking shall be observed at a bend angle of $\alpha \le (45/d^{0.7} + 20)^\circ$.

2 Specification of the intended use in accordance with the applicable EAD

The screws are used for connections in load bearing timber structures between members, softwood and hardwood of: Solid timber, glued laminated timber, cross-laminated timber (CLT) and laminated veneer lumber, similar glued members, wood-based panels or steel. "fischer Power-Fast II" screws with a thread over the full length can also be used as tensile or compressive reinforcement perpendicular to the grain or as shear reinforcement. Furthermore "fischer Power-Fast II" screws with diameter of 6 mm may also be used for fixing of thermal insulation on rafters and on vertical facades. Steel plates and wood-based panels except solid wood panels and EGGER Eurostrand OSB 4 TOP, laminated veneer lumber and CLT, shall only be fixed on the side of the screw head.

The following wood-based panels may be used:

- Plywood according to EN 636 or European Technical Assessment or national provisions that apply at the installation site
- Particleboard according to EN 312 or European Technical Assessment or national provisions that apply at the installation site
- Oriented Strand Board according to EN 300 or European Technical Assessment or national provisions that apply at the installation site
- Fibreboard according to EN 622-2 and 622-3 or European Technical Assessment (minimum density 650 kg/m³) or national provisions that apply at the installation site
- Cement bonded particleboard according to EN 634 or European Technical Assessment or national provisions that apply at the installation site
- Solid wood panels according to EN 13353 or European Technical Assessment or national provisions that apply at the installation site
- Wood-based panels for use in constructions according to EN 13986
- Cross laminated timber according to European Technical Assessment
- Laminated Veneer Lumber according to EN 14374 or European Technical Assessment
- Engineered wood products according to European Technical Assessment, provided that the ETA for the product provides provisions for the use of selftapping screws and these provisions are applied

The screws shall be driven into softwood and hardwood with a maximum characteristic density of 730 kg/m³ without pre-drilling or after pre-drilling (see Table 1 and Table 2) with a diameter not larger than the inner thread diameter for the length of the threaded part and with a maximum of the smooth shank diameter for the length of the smooth shank.

Tuble 1. Recommended pre-uriting diameters					
Nominal diameter	Bore-hole diameter [mm]				
d [mm]	Softwood Hardwood				
3,0	2,0	2,5			
3,5	2,0	2,5			
4,0	2,5	3,0			
4,5	2,5	3,0			
5,0	3,0	3,0			
6,0	4,0	4,0			

Table 1: Recommended pre-drilling diameters

Recommended values without pre-drilling for the maximum penetration length of the threaded part of "fischer Power-Fast II" made of carbon steel in wood based members like ash, beech and oak or LVL

according to ETA-14/0354 (e.g. Baubuche) are shown in Table 2.

 Table 2: Recommended penetration length without predrilling in hardwood

Nominal diameter	Maximum penetration		
d [mm]	length [mm]		
3,0	40		
3,5	45		
4,0	50		
4,5	60		
5,0	70		
6,0	70		

The hole diameter in steel members must be pre-drilled with a suitable diameter.

In connections with screws with countersunk head according to Annex A the head must be flush with the surface of the connected structural member. A deeper countersunk is not allowed.

Pan head screws according to Annex A may be used together with washers according to EN ISO 7094.

The intended use of the screws is in timber connections for which all requirements of mechanical resistance, stability and safety in use in the sense of the Basic Works Requirements 1 and 4 of Regulation 305/2011 (EU) shall be fulfilled.

"fischer Power-Fast II" screws with $d \ge 4,5 \text{ mm}$ can be driven in with standard screw driver and with impact screw drivers too (e.g. fischer FSS 18V 400 BL or fischer FSS 18V 600). It is also recommended to use, especially in combination with steel plates, torque controlled tools e.g. torque wrenches.

The design of the connections shall be based on the characteristic load-carrying capacities of the screws.

The design capacities shall be derived from the characteristic capacities in accordance with Eurocode 5 or an appropriate national code. The screws are intended for use for connections subject to static or quasi-static loading.

The zinc-coated screws are for use in timber structures subject to the moisture content of internal conditions defined by the service classes 1 and 2 regarding to EN 1995-1-1:2014.

The provisions made in this European Technical Assessment are based on an assumed intended working life of the screws of 50 years.

The indications given on the working life cannot be interpreted as a guarantee given by the producer or Assessment Body, but are to be regarded only as a means for choosing the right products in relation to the expected economically reasonable working life of the works.

Characteristic		Assessment of characteristic		
3.1	Mechanical resistance and stability*) (BWR1)		
Tensi	le strength		Characteristic value	$f_{tons k}$
1 01101		Power-Fast II	d=3,0 mm	3,2 kN
			d = 3,5 mm	4,1 kN
			d = 4,0 mm	5,2 kN
			d = 4,5 mm	6,3 kN
			d = 4,5 mm d = 5,0 mm	
				8,9 kN
			d= 6,0 mm	13,1 kN
Torsi	onal strength		Ratio of the charact	eristic torsional strengt
	C		to the mean insertio	
			$f_{tor,k} / R_{tor,mean} \ge 1,5$	
			Characteristic value	from h
		Power-Fast II	d=3,0 mm	1,5 Nm
		1 Owel-1 ast II	d=3,5 mm	2,0 Nm
			d = 4,0 mm	3,0 Nm
			· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
			d = 4,5 mm	4,2 Nm
			d= 5,0 mm	6,0 Nm
			d= 6,0 mm	10,0 Nm
3.2	Safety in case of fire (BWR2)			
React	ion to fire		performance class	603/EC, amended b
3.3	Safety in use (BWR4)		See aspects covered	l by BWR1
3.4	General aspects related to the perfor product ^{*)}	rmance of the	satisfactory durabi when used in time timber species des	een assessed as having ility and serviceabilit per structures using th cribed in EN 1995-1- conditions defined b d 2.
Identi	fication		See Annex A	
	al and special application area		See Annex B	
*) 800	additional information in section 3.5 to 3	37		

3 Performance of the product and references to the methods used for its assessment

3.5 Mechanical resistance and stability

The load-carrying capacities for the "fischer Power-Fast II" screws are applicable to the wood-based materials mentioned in paragraph 1 even though the term "timber" has been used in the following. European Technical Assessments for structural members or wood-based panels must be considered if applicable.

The characteristic lateral load-carrying capacities and the characteristic axial withdrawal capacities of "fischer Power-Fast II" screws should be used for designs in accordance with Eurocode 5 (EN 1995-1-1) or an appropriate national code.

Reductions in the cross-sectional area caused by "fischer Power-Fast II" screws shall be taken into account in accordance to the Eurocode 5.

3.5.1 Lateral load-carrying capacity

The characteristic lateral load-carrying capacity of "fischer Power-Fast II" screws shall be calculated according to EN 1995-1-1. The contribution of the rope effect may be considered. For the calculation of the load-carrying capacity, the following parameters should be taken into account.

3.5.1.1 Embedment strength $f_{h,\alpha,k}$ for the use in Solid timber

The embedment strength for "fischer Power-Fast II" screws in non-pre-drilled holes arranged at an angle between load and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$ can be calculated with the help of equation (1).

$$f_{h,\alpha,k} = \frac{0,065 \cdot \rho_k \cdot d^{-0,3}}{k_{90} \cdot \sin^2 \alpha + \cos^2 \alpha}$$
(1)

The embedment strength for "fischer Power-Fast II" screws in pre-drilled holes arranged at an angle between screw axis and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$ can be calculated with the help of equation (2).

$$f_{h,\alpha,k} = \frac{0,065 \cdot \rho_k \cdot (1 - 0,022 \cdot d)}{k_{90} \cdot \sin^2 \alpha + \cos^2 \alpha}$$
(2)

Note: Due to the modified equations it is possible to do the total calculation to determine the shear capacity with the nominal diameter d. By doing so also in the EN 1995-1-1:2014 chapter 8.2, in the "Theorie of Johansen" the nominal diameter d should be used. As long as the core diameter d_1 is less than 6 mm the influence of the angle between load and grain direction must normally not be considered. It is also possible to carry out the calculation with the inner diameter of the thread d_1 and use the equations in clause 8.3.1 in the EN 1995-1-1:2014.

With

$$k_{90} = \begin{cases} 1,35 + 0,015 \cdot d & \text{for softwood} \\ 1,30 + 0,015 \cdot d & \text{for LVL}^* \\ 0,90 + 0,015 \cdot d & \text{for hardwood} \end{cases}$$
(3)

* made from softwood or hardwood

Where

 α Angle between load and the grain direction [°]

 $f_{h,\alpha,k}$ Characteristic embedment strength [N/mm²]

 ρ_k Characteristic timber gross density [kg/m³]

d Nominal diameter of the screw [mm];

3.5.1.2 Embedment strength $f_{h,\alpha,k}$ for the use in Cross-Laminated-Timber



Figure 1: Notations CLT-elements

- (1) Element plane
- (2) Plane surface
- (3) Edge surface (narrow side)
- (4) Inner layer (lamellas)
- (5) Outer layer (lamellas)
- (6) Middle layer (lamella)

If there are no other technical specification (ETA or hEN) for CLT, the embedment strength for screws can be calculated as following. The following specifications are only for screws with a diameter of at least 6 mm, otherwise possible influences of gaps between the single lamellas have to be considered.

Screws in the plane surface

The embedment strength for screws in the plane surface of CLT-elements should be assumed as for solid timber according to equation (1) or (2), based on the characteristic density of the outer layer. If relevant, the angle between force and grain direction of the outer layer should be considered.

Screws in the narrow (edge) side

The embedment strength for screws in the narrow side of CLT-elements should be assumed according to equation (4).

$$f_{h,k} = 20 \cdot d^{-0.5} \tag{4}$$

3.5.1.3 Embedment strength $f_{h,\alpha,k}$ for the use in LVL (ETA-14/0354)

The embedment strength for "fischer Power-Fast II" screws with $d \ge 5$ mm arranged at an angle between load and grain direction, $0^{\circ} \le \alpha \le 90^{\circ}$ can be calculated with the help of equation (5) in direction 90|90 (see figure 2).

$$f_{h,\alpha,k} = \frac{f_{h,0,k}}{(0,9+0,037 \cdot d) \cdot \sin^2 \alpha + \cos^2 \alpha}$$
(5)

With

3.5.1.4 Effective number of screws per row nef

For laterally loaded screws, the rules for multiple fastener connections in EN 1995-1-1 should be applied.

3.5.2 Yield strength $f_{y,Rk}$

The characteristic yield strength of the different screw types of "fischer Power-Fast II" can be taken into account as shown below.

$$f_{y,Rk} = 1050 \text{ N/mm}^2$$
 (6)

3.5.3 Yield moment M_{y,Rk}

The characteristic yield moment shall be calculated with the help of equation (7)

$$M_{\nu Rk} = 0.15 \cdot 600 \cdot d^{2.65} \tag{7}$$

Where

 $M_{y,Rk}$ Characteristic yield moment [Nmm]dNominal diameter of the threaded part
[mm]

3.5.4 Axial withdrawal capacity

The axial withdrawal capacity is limited by the head pull-through capacity, the withdrawal capacity and the tensile or compressive capacity of the screw. For "fischer Power-Fast II" fully threaded screws, the withdrawal capacity of the thread in the member with the head may be taken into account instead of the head pull-through capacity.

3.5.4.1 Withdrawal capacity $F_{ax,\alpha,Rk}$ Solid timber and Glued Laminated, Timber (EN 338, EN 14080) and LVL (ETA-14/0354)

The characteristic withdrawal capacity in softwood of "fischer Power-Fast II" screws with an angle of $0^{\circ} \le \alpha \le 90^{\circ}$ shall be calculated according to equation (8). For screws with an outer diameter d $\le 5,0$ mm equation (8) is only valid for $45^{\circ} \le \alpha \le 90^{\circ}$.

$$F_{ax,\alpha,Rk} = n_{ef} \cdot k_{ax} \cdot f_{ax,90,k} \cdot d \cdot l_{ef} \cdot \left(\frac{\rho_k}{350}\right)^{0.8}$$
(8)

With

$$k_{ax} = \min \begin{cases} 0,3 + (0,7 \cdot \alpha) / 45^{\circ} \\ 1,00 \end{cases}$$
(9)

According to equation (10) the point side penetration length has to be considered between the following range.

$$l_{ef} = \min \begin{cases} \frac{4 \cdot d}{\sin \alpha} \\ 20 \cdot d \end{cases}$$

(10) Where

d Outer thread diameter [mm]

 l_{ef} Penetration length of the threaded part according to EN 1995-1-1; For fully threaded screws the thread length including the head length in [mm]

 α Angle between grain and screw axis [°]

- ρ_k Characteristic timber gross density, maximum 730 kg/m³ [kg/m³]
- $F_{ax,\alpha,Rk}$ Characteristic withdrawal capacity of the screw with an angle α to the grain [N]
- n_{ef} Effective number of screws according to EN 1995-1-1:2014
- $f_{ax,90,k}$ Characteristic withdrawal parameter as following.

Power-Fast II	in solid timber or		
	glued laminated timber		
d= 3,0 mm	$f_{ax,90,k} =$	15,5 N/mm ²	
d= 3,5 mm	$f_{ax,90,k} =$	14,9 N/mm ²	
d= 4,0 mm	$f_{ax,90,k} =$	14,5 N/mm ²	
d= 4,5 mm	$f_{ax,90,k} =$	14,1 N/mm ²	
d= 5,0 mm	$f_{ax,90,k} =$	13,8 N/mm ²	
d= 6,0 mm	$f_{ax,90,k} =$	12,9 N/mm ²	



Figure 2: Power-Fast II in hardwood LVL

The characteristic withdrawal capacity in hardwood LVL according to ETA-14/0354 of "fischer Power-Fast II" screws with an angle of $0^{\circ} \le \alpha \le 90^{\circ}$ shall be calculated according to equation (8). For screws with an outer diameter d $\le 5,0$ mm equation (8) is only valid for $45^{\circ} \le \alpha \le 90^{\circ}$.

$$F_{ax,\alpha,Rk} = n_{ef} \cdot k_{ax} \cdot f_{ax,\alpha|\alpha,k} \cdot d \cdot l_{ef} \cdot \left(\frac{\rho_k}{730}\right)^{0,8}$$
(11)

With

$$k_{ax} = \min \begin{cases} 0.3 + (0.7 \cdot \alpha) / 45^{\circ} \\ 1.00 \end{cases}$$
(12)

3.5.4.2 Withdrawal capacity *F*_{ax,Rk} EGGER Eurostrand OSB 4 TOP

The characteristic axial withdrawal capacity of "fischer Power-Fast II" screws in EGGER Eurostrand OSB 4 TOP with an angle of $\alpha = 90^{\circ}$ and a thickness of at least 12 mm can be calculated according to equation (8), with

$$f_{ax,90,OSB,Rk} = 10 \text{ N/mm}^2$$
 (13)

for "fischer Power-Fast II" screws with diameter $d \ge 5$ mm (see Egger Eurostrand OSB 4 TOP).

3.5.4.3 Withdrawal capacity $F_{ax,Rk}$ Cross laminated timber

If there are no other technical specification (ETA or hEN) for cross laminated timber (CLT), the withdrawal capacity for screws can be calculated as following.

Screws in the plane surface

The withdrawal capacity for screws with $d \ge 6$ mm in the plane surface of CLT-elements should be assumed as for solid timber according to equation (8) based on a characteristic density of equation (14), if there are no other specifications are given. If necessary gaps between the single lamellas have to be considered.

$$\rho_k = 1, 1 \cdot \rho_{lav,k} \tag{14}$$

With

 $\rho_{\text{lay},k}$ Lowest characteristic density of the lamella in the CLT-element [kg/m³]

Screws in the narrow side

The withdrawal capacity for screws in the narrow side of CLT-elements should be assumed according to equation (15).

$$F_{ax,Rk} = 20 \cdot d^{0,8} \cdot l_{ef}^{0,9}$$
(15)

Screws in the narrow side should be driven perpendicular into the grain of the lamella. The penetration length has to be at least $3 \cdot d + l_{ef}$.

If it is guaranteed that the angle between the lamellas and the screw axis is $\ge 30^{\circ}$ the characteristic withdrawal capacity from equation (15) can be increased of about 25 %.

For screws penetrating more than one layer of cross laminated timber, the different layers may be taken into account proportionally.

3.5.4.4 Effective number of screws n_{ef}

For axially loaded screws in tension, where the external force is parallel to the screw axis, the rules in EN 1995-1-1, 8.7.2 (8) should be applied.

$$n_{ef} = n^{0.9}$$
 (16)

For inclined screws in timber-to-timber or steel-to timber shear connections, where the screws are arranged under an angle $30^{\circ} \le \alpha \le 60^{\circ}$ between the shear plane and the screw axis, the effective number of screws n_{ef} should be determined with equation below.

$$n_{ef} = \max \begin{cases} n^{0.9} \\ 0.9 \cdot n \end{cases}$$
(17)

With

n Pieces of (inclined/cross pairs) screws in a row parallel to the grain

For screws as compression reinforcement or inclined screws as fasteners in mechanically jointed beams or columns $n_{ef} = n$.

3.5.5 Head pull-through capacity *f_{head,k}* Solid timber and Glued Laminated Timber (EN 338, EN 14080) and LVL (ETA-14/0354)

The characteristic head pull-through capacity of "fischer Power-Fast II" screws in solid timber can be calculate as following.

$$F_{ax,\alpha,Rk} = n_{ef} \cdot f_{head,k} \cdot d_h^2 \cdot \left(\frac{\rho_k}{350}\right)^{0.8}$$
(18)

For timber elements with a thickness of at least 20 mm, the characteristic value of the head pull-through parameter $f_{head,k}$ can be taken into account as following.

Power-Fast II	in solid timber, cross laminated				
	timber, glued laminated timber				
	and LVL				
d= 3,0 mm	$d_h=6,0 \text{ mm}$	$f_{head,k}$ =19,0 N/mm ²			
d= 3,5 mm	d _h = 7,0 mm	fhead,k=16,3 N/mm ²			
d= 4,0 mm	d _h = 8,0 mm	$f_{head,k}$ =15,0 N/mm ²			
d= 4,5 mm	d _h = 8,8 mm	$f_{head,k}$ =14,2 N/mm ²			
d= 5,0 mm	d _h = 9,8 mm	$f_{head,k}$ =13,4 N/mm ²			
d= 6,0 mm	d _h =11,8mm	$f_{head,k}$ =13,0 N/mm ²			

3.5.6 Head pull-through capacity *f*_{head,k} Wood based panels

For the following wood-based panels described in chapter 1 with a thickness of more than 20 mm the head pull-through parameter can constitute with

$$f_{head,k} = 10 \text{ N/mm}^2 \tag{19}$$

For wood-based panels with a thickness between 12 mm and 20 mm the characteristic value of the head pull-through parameter can calculate with

$$f_{head,k} = 8 \text{ N/mm}^2 \tag{20}$$

For wood based panels with a thickness of less than 12 mm the characteristic head pull-through capacity shall be calculated with $f_{head,k}=8 N/mm^2$ with a limit of 400 N complying with a minimum thickness of the wood

based panels of $1,2 \cdot d$. In addition, to apply the minimum thickness of *Table 3*.

Table 3: Minimum	thickness	of w	ood b	pased	panels
			2.4	.1 .	1

Wood based panel	Min. thickness
wood based panel	[mm]
Plywood	6
Oriented Strand board OSB	8
Solid wood panels	12
Particleboards	8
Cement bonded particle boards	8
Fibreboards (hardboards and	6
medium boards)	0

3.5.7 Tensile capacity *f*_{tens,k}

The characteristic tensile capacity $f_{tens,k}$ of "fischer Power-Fast II" screws depending on the outer diameter is for

Power-Fast II		
d= 3,0 mm	$f_{tens,k} =$	3,2 kN
d= 3,5 mm	$f_{tens,k} =$	4,1 kN
d= 4,0 mm	$f_{tens,k} =$	5,2 kN
d= 4,5 mm	$f_{tens,k} =$	6,3 kN
d= 5,0 mm	$f_{tens,k} =$	8,9 kN
d= 6,0 mm	$f_{tens,k} =$	13,1 kN

The tear-off capacity of the screw head is greater than the tensile capacity of the screw.

3.5.8 Compression capacity

The design compressive capacity $F_{ax,Rd}$ of "fischer Power-Fast II" screws with full thread along the length embedded in timber shall be calculated as following.

 $F_{ki,Rd} = \kappa_c \cdot N_{pl,d}$

$$F_{ax,Rd} = \min \begin{cases} F_{ax,Rd} \\ F_{ki,Rd} \end{cases}$$
(21)

(22)

Where $F_{ax Rd}$

$$F_{ax,Rd}$$
According to equation (8) $F_{ki,Rd}$ According to equation (22)

With

$$\kappa_c = 1 \qquad \text{for } \lambda_k \le 0,2$$

$$\kappa_c = \frac{1}{k + \sqrt{k^2 - \overline{\lambda}^2}} \qquad \text{for } \overline{\lambda}_k > 0,2 \qquad (23)$$

 $f_{am} = \frac{1}{2} < 0.2$

and

$$k = 0,5 \cdot \left[1 + 0,49 \cdot \left(\overline{\lambda}_k - 0,2\right) + \overline{\lambda}_k^2\right]$$
(24)

The relative slenderness ratio shall be calculated with

$$\overline{\lambda}_k = \sqrt{\frac{N_{pl,k}}{N_{ki,k}}} \tag{25}$$

With the characteristic value for the axial capacity in case of plastic analysis referred to the outer thread diameter

$$N_{pl,k} = \frac{(0,7 \cdot d)^2 \cdot \pi}{4} \cdot f_{y,Rk}$$
(26)

And the characteristic ideal elastic buckling load

$$N_{ki,k} = \sqrt{c_h \cdot E_s \cdot I_s} \tag{27}$$

With the

Elastic foundation of the screw:

$$c_h = (0,19+0,0084 \cdot d) \cdot \rho_k \cdot \left(\frac{\alpha}{180^\circ} + 0,5\right)$$
 (28)

Modulus of elasticity:

$$E_{\rm s} = 210.000 \, \rm N/mm^2$$
 (29)

Second moment of area:

$$I_{s} = \frac{\pi \cdot (0, 7 \cdot d)^{4}}{64}$$
(30)

Note: The compressive capacity must be modified for $f_{ax,d}$ with the factors k_{mod} and γ_M for timber according to EN 1995-1-1 while $N_{pl,d}$ the partial-factor $\gamma_{M,1}$ for steel buckling according to EN 1993-1-1 and/or national standards respectively have to be considered.

3.5.9 Combined laterally and axially loaded screws

For connections subjected to a combination of axial and lateral load, the following expression has to be considered according to equation

$$\left(\frac{F_{ax,Ed}}{F_{ax,Rd}}\right)^2 + \left(\frac{F_{\nu,Ed}}{F_{\nu,Rd}}\right)^2 \le 1$$
(31)

With

 $F_{ax,Ed}$ Axial design action [N] $F_{v,Ed}$ Lateral design action [N] $F_{ax,Rd}$ Design load-carrying capacity of an axially
loaded screw [N]

$F_{v,Rd}$ Design load-carrying capacity of a laterally loaded screw [N]

3.5.10 Slip modulus

Laterally loaded screws

For laterally loaded "fischer Power-Fast II" screws the slip modulus predrilled or non-predrilled for the serviceability limit state (SLS) for screws could be calculated according to EN 1995-1-1:2014 independent of the angle α to the grain with equation (32).

$$K_{ser} = k_{sys} \cdot k_{sb} \cdot \frac{\rho_m^{1,5} \cdot d}{23}$$
(32)

With

 k_{sys} $k_{sys} = \begin{cases} 1 & \text{for timber-timber connections} \\ 2 & \text{for steel-timber connections} \end{cases}$ k_{sb} Number of shear bands



Figure 3: Definition shear bands

Where

 K_{ser} Slip modulus in SLS [N/mm] ρ_m Mean timber density [kg/m³]

Axially loaded screws

For axially loaded screws the slip modulus for the serviceability limit state (SLS) could be calculated independent on the angle α to the grain according to equation (33).

$$K_{ser} = 25 \cdot d \cdot l_{ef} \tag{33}$$

To consider the slip modulus K_u in the ultimate limit state (ULS) K_{ser} has to be reduced for both directions (laterally and axially) according to EN 1995-1-1.

$$K_u = 2/3 \cdot K_{ser} \tag{34}$$

3.5.12 Minimum timber cross section, end- and edge distances

For structural timber members, minimum spacing and distances for screws in predrilled holes are given in EN 1995-1-1:2014 clause 8.3.1.2 and table 8.2 as for nails

in predrilled holes. Here, the outer thread diameter d must be considered.

For screws in non-predrilled holes, minimum spacing and distances are given in EN 1995-1-1:2014 clause 8.3.1.2 and table 8.2 as for nails in non-predrilled holes.

Minimum thickness for structural members are in general t=24 mm.

3.5.12.1 Solid timber (EN 338, EN 14080)

Alternatively, minimum distances and spacing for exclusively axially loaded "fischer Power-Fast II" screws in non-predrilled holes in members of solid timber (softwood and hardwood), glued laminated timber or similar glued products (softwood and hardwood) with a minimum thickness $t = 12 \cdot d$ and a minimum width of 8·d or 60 mm, whichever is the greater, may be taken as:

Spacing a ₁ parallel to the grain of solid timber	$a_1 = 5 \cdot d$
Spacing a ₂ perpendicular to the grain of solid timber	$a_2 = 5 \cdot d$
Distance $a_{3,c}$ from centre of the screw-part in timber to the end grain of solid timber	$a_{3,c}=9\cdot d$
Distance a _{4,c} from centre of the screw-part in timber to the edge of solid timber	a. – 4.d
	$a_{4,c} = 4 \cdot d$

Spacing a_2 perpendicular to the grain may be reduced from 5·d to 2,5·d, if the condition $a_1 \cdot a_2 \ge 25 \cdot d^2$ is fulfilled. For Douglas fir members minimum spacing and distances parallel to the grain shall be increased by 50%.

Minimum distances from the unloaded edge perpendicular to the grain may be reduced to $3 \cdot d$ also for timber thickness t < $5 \cdot d$, if the spacing parallel to the grain and the end distance is at least $25 \cdot d$.

3.5.12.2 Cross Laminated Timber

Unless specified otherwise in the technical specification (ETA or hEN) of cross laminated timber (CLT), minimum distances and spacing for screws in the plane surface of cross laminated timber members with a minimum thickness $t = 10 \cdot d$ may be taken as (see Annex B2).

Spacing a_1 parallel to the grain of	4 1
the CLT-plane surface	$a_1 = 4 \cdot d$
Spacing a ₂ perpendicular to the	
grain of the CLT-plane surface	$a_2 = 2, 5 \cdot d$
Distance a _{3,c} from centre of the	
screw-part in CLT to the unloaded	
end grain of the plane surface	$a_{3,c}=6\cdot d$
Distance a _{3,t} from centre of the	
screw-part in CLT to the loaded	
end grain of the plane surface	$a_{3,t} = 6 \cdot d$
Distance a _{4,c} from centre of the	
screw-part in CLT to the unloaded	
edge of the plane surface	$a_{4,c} = 2,5 \cdot d$
Distance a _{4,t} from centre of the	
screw-part in CLT to the loaded	
edge of the plane surface	$a_{4,t} = 6 \cdot d$

Unless specified otherwise in the technical specification (ETA or hEN) of cross laminated timber, minimum distances and spacing for screws in the edge surface of cross laminated timber members with a minimum thickness t = 10 d and a minimum penetration depth perpendicular to the edge surface of 10 d may be taken as (see Annex B2):

Spacing a ₁ parallel to the CLT edge surface	$a_1 = 10 \cdot d$
Spacing a ₂ perpendicular to the CLT edge surface	$a_2 = 4 \cdot d$
Distance $a_{3,c}$ from centre of the screw- part in CLT to the unloaded end grain of the edge surface	$a_{3,c} = 7 \cdot d$
Distance $a_{3,t}$ from centre of the screw- part in CLT to the loaded end grain of the edge surface	$a_{3,t} = 12 \cdot d$
Distance a _{4,c} from centre of the screw- part in CLT to the unloaded edge surface	$a_{4,c} = 3 \cdot d$
Distance a _{4,t} from centre of the screw- part in CLT to the loaded edge surface	$a_{4,t} = 6 \cdot d$

For a crossed screw couple the minimum spacing between the crossing screws is $1,5 \cdot d$.

3.6 Aspects related to the performance of the product

3.6.1 Corrosion protection in service class 1 and 2

The "fischer Power-Fast II" screws are produced from carbon steel. They are zinc-plated (e.g. yellow-zinced or blue-zinced), bonus-zinc-coated, burnished, nickel-plated or brass-plated. The mean thickness of the zinc-plated screws is min. 5 μ m.

3.7 General aspects related to the intended use of the product

The screws are manufactured in accordance with the provisions of the European Technical Assessment using the automated manufacturing process as identified during the inspection of the plant by the assessment body issuing the ETA and the notified body and laid down in the technical documentation. The installation shall be carried out in accordance with Eurocode 5 or an appropriate national code unless, otherwise defined in the following.

4 Attestation and verification of constancy of performance (AVCP)

4.1 AVCP system

According to the decision 97/176/EC of the European Commission1, as amended, the system(s) of assessment and verification of constancy of performance (see Annex V to Regulation (EU) No 305/2011) is 3.

Appendix 12 / 22







Appendix 14 / 22

Power-Fast II - Self-drilling screw - Pan head with full- or partial thread															
						ls ²⁾									
			-	•		lgf		-							
	U	Inderhead nilling pocl	kets ¹⁾	-								ade mark-	~		
				6											
			- ਚ ਿ	A A A	fort.	****	TASA	190 -	o o				60.)	
			I L	/		~ ~ ~ ~ ~	lgp			Drive					
		Shank	ribs ¹⁾	-/			-51-		oremiller ¹⁾	Drive	PZ		Drive T	x	
¹⁾ optional													F	igure not	to scale
	bon Ste sible s		reatments:					lated, b	lue zinc·	-plated 2	≥12µm,	bonus-z	inc-coa	ted, bur	nished,
Nor	ninal	diame	tor		plated, t			4	0	4	5	6	0	6	0
			t er liameter		,0 00		,5 50		,0 00		,5 50		,0 00		,0 00
d —		deviatio		± 0),25	± 0	,25	± 0	,30		,30		,30	± 0	,30
d4 —		hread di			95		20		50		75		25		95
		deviatio diamete),18 00		0,18 00		,20 00		,20 00		,20 ,00		,20 ,00
d h –		deviatio),50	-	,50		00 ,60		,60		,60 ,60		,60 ,60
d- –		diamete			25		60		90		20		70		30
-	Allow. Head I	deviatio	on),15 30		,15 50		,15 80		,15 80		,15 40		,15 40
		ve TX			0	10	20		20		0	20	25		0
		ve PZ			1	2		2			2		2		3
		ength l	s ²⁾	Star	ndard th	read le	ength I	l _{gf} = Ful	l threac	1 l _{gp} =	Partial	thread	Tolera	nce: ±	2,0 ³⁾
Nomin lengtl		min	max	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}	l _{gf}	l _{gp}
20 25		<u>, –1,05</u>	ls +1,05	16 21	18	16 21	18	20	18	20					
30		<u>, –1,25</u> , –1,25	l₅ +1,25 l₅ +1,25	21	18	21	18	20	18	20	18	24			
35		s —1,50	ls +1,50	31	24	31	24	30	24	30	24	29	24	28	
40		s –1,50	ls +1,50	36	28	36	28	35	28	35	28	34	28	33	28
45 50		<u>,</u> –1,50 , –1,50	l₅ +1,50 l₅ +1,50	41	30	41 46	30 30	40 45	30 30	40 45	30 30	39 44	30 30	38 43	30 30
55		, <u>1,86</u> , –1,75	ls +1,75					50	36	50	36	49	36	48	48
60		, –1,75	ls +1,75					55	36	55	36	54	36	53	36
70 80		<u>-1,75</u>	l₅ +1,75 l₅ +1,75						42 45	65 75	42 45	64 74	42 45	63 73	42 45
90			$l_{s} + 1,73$ $l_{s} + 2,00$						40	13	40	/ +	45 54	13	45 54
100		, –2,00											60		60
110			ls +2,00										70		70
120 in		<u>-2,00</u> of 10mr	l₅ +2,00 m										70		70
130-30		s –3,00													70
Table A	3.1: Sc	rew size	es and mat	terial									All	sizes in	mm
²⁾ Other length	Table A3.1: Screw sizes and material All sizes in mm ■ Screws with partial thread > 60 mm l _s with shank ribs 2) Other screw lengths with l _s min ≤ l _s ≤ l _s max and other thread lengths l _{gf} resp. l _{gp} ≥ 4xd up to max, standard thread lengths are allowed 3) For 10mm ≤ l _{gf} resp. l _{gp} ≤ 18mm → tolerance ±1,5mm and for 18mm < l _{gf} resp. l _{gp} ≤ 30mm → tolerance ±1,7mm														
			fi	scher	Powe	er-Fast	t II					ļ	Annex	A3	
			Sc	rew si	zes an	d mate	erial								







Design of the battens

The bending stresses of the battens are calculated with

$$M_{Ed} = \frac{\left(F_{Ed} + F_{s,Ed}\right) \cdot l_{char}}{4}$$

Where

Where		
F _{Ed} F _{s,Ed} M _{Ed} l _{char}	Point loads perpendicular to the battens [N] Point loads perpendicular to the battens in the area of the so Design bending moment of the batten [Nmm] Characteristic length of the batten [mm]	rew heads [N]
	with $l_{char} = \sqrt[4]{\frac{4 \cdot EI}{w_{ef} \cdot K}}$, where	
	<i>EI</i> Bending stiffness of the batten [Nmm ²] w_{ef} Effective width of the thermal insulation [mm] with $w_{ef} = w + t_{ti} / 2$, where	
	wMimimum width of the batten or rafter [mm] t_{ii} Thickness of the thermal insulation [mm]KBedding modulus [N/mm³]The coefficient K may be calculated from the model E_{ii} and the thickness t_{ii} of the thermal insulation ifwidth w_{ef} of the thermal insulation under compressDue to the load extension in the insulation the efficient than the width of the batten or rafter, respfurther calculations, the effective width w_{ef} of the thermal	the effective sion is known. Tective width w_{ef} is pectively. For
	may be determined with $K = \frac{E_{ti}}{t_{ri}}$, where	
	E_{ti} Modulus of elasticity of the thermal insulation t_{ti} Thickness of the thermal insulation [mm]	[N/mm²]
The follow	ving conditions shall be satisfied:	
a) - Where	$\frac{\sigma_{m,Ed}}{f_{m,d}} \le 1$	
$\sigma_{m,Ed} \ f_{m,d}$	Design value of the bending stress of the batten [N/mm²] Design value of the bending strength [N/mm²]	
	$\frac{\tau_{Ed}}{f_{v,d}} = \frac{3 \cdot V_{Ed}}{2 \cdot A_{ef} \cdot f_{v,d}} \le 1$	
Where $f_{v,d}$ A_{ef} V_{Ed}	Design value of the shear strength of the batten [N/mm ²] Net cross section of the batten [mm ²] Design shear load onto the batten [N] with $V_{Ed} = \frac{F_{Ed} + F_{s,Ed}}{2}$	
$ au_{Ed}$	Design value of the shear stress of the batten [N/mm²]	
	fischer Power-Fast II	Annex B1.4
	Fixing of on-roof insulation	

Design of the heat insulation

The compressive stresses in the thermal insulation shall be calculated with

$$\sigma_{c,Ed} = \frac{1, 5 \cdot F_{Ed} + F_{s,Ed}}{2 \cdot l_{char} \cdot w_{ef}}$$

Where

	Fixing of on-roof insulation	
	fischer Power-Fast II	Annex B1.4
	% deformation calculated according to EN 826.	·
Note: The de	$\sigma_{c,Ed}$ is sign value of the compressive stress shall not be greater than	110 % of the compressive
$\sigma_{c,Ed}$	E_{ti} Modulus of elasticity of the thermal insulation t_{ti} Thickness of the thermal insulation [mm] Design value of the compression stresses of the thermal insulation	
	may be determined with $K = \frac{E_{ti}}{t_{ti}}$, where	
	E_{ti} and the thickness t_{ti} of the thermal insulation if width w_{ef} of the thermal insulation under compres Due to the load extension in the insulation the eff greater than the width of the batten or rafter, resp further calculations, the effective width w_{ef} of the t	the effective sion is known. ective width w_{ef} is pectively. For
	with $w_{ef} = w + t_{ti} / 2$, wherew Mimimum width of the batten or rafter [mm] t_{ti} Thickness of the thermal insulation [mm]KBedding modulus [N/mm³]The coefficient K may be calculated from the mode	dulus of elasticity
	EIBending stiffness of the batten [Nmm²] w_{ef} Effective width of the thermal insulation [mm]with w_{ef}	
	with $l_{char} = \sqrt[4]{\frac{4 \cdot EI}{w_{ef} \cdot K}}$, where	
F _{Ed} F _{s,Ed} l _{char}	Point loads perpendicular to the battens [N] Point loads perpendicular to the battens in the area of the sc Characteristic length of the batten [mm]	rew heads [N]

Design of the screws

The screws are loaded predominantly axially. The axial tension force in the screw may be calculated from the shear loads of the roof

$$F_{ax,Ed} = \frac{R_{s,Ed}}{\cos \alpha_r} \le F_{ax,\alpha,Rd}$$

Where

 $F_{ax,Ed}$ Design value of the axial tension forces onto the screw [N] $F_{ax,\alpha,Rd}$ Design value of the withdrawal capacity of the screw [N] $R_{s,Ed}$ Shear loads onto the screw [N] α_r Angle inclined screw (see figure B1.3) [°]

The load-carrying capacity of axially loaded screws is the minimum design value of the axial withdrawal capacity of the threaded part of the screw, the head pull-through capacity of the screw and the tensile capacity of the screw.

In order to limit the deformation of the screw head for heat insulation thicknesses over 200 mm or with compressive strength below $0,12 \text{ N/mm}^2$, respectively, the axial withdrawal capacity of the screws shall be reduced by the factors k_1 and k_2 .

$$F_{ax,\alpha,Rd} = \min\left\{k_{ax} \cdot f_{ax,d} \cdot d \cdot l_{ef} \cdot k_1 \cdot k_2 \cdot \left(\frac{\rho_k}{350}\right)^{0,8}, f_{head,d} \cdot d_h^{-2} \cdot \left(\frac{\rho_k}{350}\right)^{0,8}, f_{tens,d}\right\}$$

Where

$F_{ax,\alpha,Rd}$	Design value of the withdrawal capacity of the screw [N]
d	Diameter of the screw [mm]
d_h	Head diameter of the screw [mm]
$f_{ax,d}$	Design value of the withdrawal parameter of the threaded part of the screw [N/mm ²]
fhead,d	Design value of the head pull-through capacity of the screw [N/mm ²]
ftens,d	Design value of the tensile capacity of the screw [N]
<i>k</i> _{ax}	Coefficient according to equation (8)
k_{I}	$min \{1; 200 / t_{ii}\}$ [-]
k_2	min {1; $\sigma_{10\%,Ed}/(0,12)$ [-], where
	$\sigma_{10\%,Ed}$ Compressive stress of the heat insulation at 10 % deformation [N/mm ²]
	<i>t_{ii}</i> Thickness of the thermal insulation [mm]
l _{ef}	Point side penetration length of the threaded part in the rafter with $l_{ef} \ge 40$ mm [mm]
ά	Angle between grain and screw axis ($\alpha \ge 30^\circ$) [°]
$ ho_k$	Characteristic density of the timber element [kg/m³]

Note: If in the equation for $F_{ax,Rd}$ the factors k_1 and k_2 are considered, the deflection of the battens does not need to be considered. Alternatively to the battens, panels with a minimum thickness of 20 mm from plywood according to

EN 636 or an ETA or national provisions that apply at the installation site, particle board according to EN 312 or an ETA or national provisions that apply at the installation site, oriented strand board according to EN 300 or an ETA or national provisions that apply at the installation site and solid wood panels according to EN 13353 or an ETA or national provisions that apply at the installation site or cross laminated timber according to an ETA may be used.

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Thermal insulation material on rafters with parallel screws perpendicular to the roof plane

Alternatively to the battens, panels with a minimum thickness of 20 mm from plywood according to EN 636, particleboard according to EN 312, oriented strand board OSB/3 and OSB/4 according to EN 300 or European Technical Approval and solid wood panels according to EN 13353 may be used.

Characteristic load-carrying capacity of a screw loaded in shear:

$$F_{v,Rk} = \min \begin{cases} f_{h,b,k} \cdot d \cdot t_{b} \\ f_{h,r,k} \cdot d \cdot t_{r} \\ \frac{f_{h,b,k} \cdot d \cdot \beta}{1+\beta} \cdot \left(\sqrt{4t_{ti}^{2} + (2+\frac{1}{\beta})t_{b}^{2} + (2+\beta)t_{r}^{2} + 4t_{ti}(t_{b} + t_{r}) + 2t_{b}t_{r}} - 2t_{ti} - t_{b} - t_{r}\right) + \frac{F_{ax,Rk}}{4} \\ 1,05 \cdot \frac{f_{h,b,k} \cdot d \cdot \beta}{\frac{1}{2} + \beta} \left(\sqrt{t_{ti}^{2} + t_{ti}t_{b} + \frac{t_{b}^{2}}{2}\left(1 + \frac{1}{\beta}\right) + \frac{M_{y,k}}{f_{h,b,k} \cdot d}\left(1 + \frac{2}{\beta}\right)} - t_{ti} - \frac{t_{b}}{2}\right) + \frac{F_{ax,Rk}}{4} \\ 1,05 \cdot \frac{f_{h,b,k} \cdot d \cdot \beta}{\frac{1}{2} + \beta} \left(\sqrt{t_{ti}^{2} + t_{ti}t_{r} + \frac{t_{r}^{2}}{2}(1 + \beta) + \frac{M_{y,k}}{f_{h,b,k} \cdot d}\left(2 + \frac{1}{\beta}\right)} - t_{ti} - \frac{t_{r}}{2}\right) + \frac{F_{ax,Rk}}{4} \\ 1,15 \cdot \frac{f_{h,b,k} \cdot d}{1+\beta} \left(\sqrt{\beta^{2}t_{ti}^{2} + 4 \cdot \beta(\beta + 1) \cdot \frac{M_{y,k}}{f_{h,b,k} \cdot d}} - \beta \cdot t_{ti}\right) + \frac{F_{ax,Rk}}{4} \end{cases}$$

Where

	with $\beta = \frac{f_{h,r,k}}{f_{h,b,k}}$	
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Fixing of on-roof insulation	Fixing of on-roof insulation	



Table B2.1: Minimum spacing, end and edge distances of screws in the **plane surfaces** of cross laminated timber

	a ₁	a _{3,t}	a _{3,c}	a ₂	a _{4,t}	a _{4,c}
Plane surface	4 · d	6 · d	6 · d	2,5 · d	6 · d	2,5 · d

Definition of spacing, end and edge distances in the **edge surface** (narrow side) unless otherwise specified in the technical specification (ETA or hEN) for the cross laminated timber.







Table B2.2: Minimum spacing, end and edge distances of screws in the **edge surfaces** (narrow side) of cross laminated timber

	a₁	a _{3,t}	a _{3,c}	a 2	a _{4,t}	a _{4,c}
Edge surface	10 · d	12 · d	7 ⋅ d	$4 \cdot d$	6 · d	3 · d

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